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PART III

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EVALUATION OF MOLECULAR WEIGHT  
FROM EQUILIBRIUM SEDIMENTATION**

**PART III. MOLECULAR WEIGHT DISTRIBUTIONS FROM  
EQUILIBRIUM SEDIMENTATION-DIFFUSION DATA  
VIA LINEAR PROGRAMMING**

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PART III

## **EVALUATION OF MOLECULAR WEIGHT FROM EQUILIBRIUM SEDIMENTATION**

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FOREWORD

This report was prepared by the Polymer Branch of the Nonmetallic Materials Division. The work was initiated under Project No. 7342, "Fundamental Research on Macromolecular Materials and Lubrication Phenomena." Task No. 734203, "Fundamental Principles Determining the Behavior of Macromolecules," with Dr. M. T. Gehatia acting as task scientist. Coauthors are Mr. R. R. Jurick, ASD Computer Science Center (ASVC), and Dr. D. R. Wiff, Research Institute, University of Dayton. The work was administered under the direction of the Air Force Materials Laboratory, Directorate of Laboratories, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio.

The report covers research conducted from September 1968 to August 1969. The manuscript was released by the authors in October 1969 for publication as a technical report.

This technical report has been reviewed and is approved.

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## ABSTRACT

Within the past decade easy access to high speed digital computers has renewed interest in deriving molecular weight distributions from sedimentation-diffusion equilibrium data. One of the computational schemes which appears most promising is the Simplex Method of linear programming. The purpose of this work was to investigate the advantages and limitations of this approach.

It was found that, even though inferring a molecular weight distribution from sedimentation-diffusion equilibrium data is mathematically an ill-posed problem, the method of linear programming yields qualitatively a good molecular weight distribution. Also, the method proved satisfactory for the case when sedimentation equilibrium data was acquired from only a single angular velocity.

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## SECTION I

### INTRODUCTION

The relationship describing sedimentation-diffusion equilibrium of an ideal polydisperse solution in an ultracentrifuge can be given by a Fredholm integral equation of the first kind (Reference 1). Since no rigorous solution of this integral is known, there have been many attempts to solve it by approximation (References 2, 3). These efforts mainly involved use of Fourier transforms or Laplace transforms by assuming an approximate functional expression for the experimental concentration gradient along the ultracentrifugal cell, or by expanding the molecular weight distribution (MWD) into a polynomial of assumed functions.

The main weakness has been that some parts of the calculated distribution would be negative. Physically, of course, we know that the MWD for any molecular weight must always be positive or zero. Recently Lee (Reference 4) carried out an investigation of the Fredholm integral equation and found that mathematically it is an "ill-posed" problem. In trying to infer a MWD from experimental measurements of concentration gradients small errors can lead to an unacceptable MWD. Therefore, we compromised in trying to determine only an "overall" shape of the MWD without being specific to individual points, i. e., we allowed certain fluctuations of the curve to be present and ignored fine structure.

To generalize a theoretical analysis, let us accept that the MWD can be slightly negative for some molecular weight values. Since we chose to ignore the point-by-point functional form of the MWD, the next logical step would be to subdivide the MWD into narrow (not infinitesimal) but finite molecular weight strips. This would result in approximations of MWD by rectangles of finite width and would lead naturally to the use of matrices. This has been done (Reference 5) but unfortunately the matrices are "ill-conditioned" or nearly singular.

Scholte (Reference 6 and 7) in 1968, still using matrices, applied the scheme of linear programming to infer a MWD from experimental measurements of concentration gradients at various angular velocities. The main

advantage to this approach is that values of the MWD are forced to be greater than or equal to zero and "slack variables" are introduced to account for experimental error. Scholte evaluated the MWD at ten molecular weights, then shifted to ten other molecular weights in a prescribed manner, continuing until, finally, there were four such sets. Since each set represented an individual solution, one quarter of the sum of the four sets also represented a solution. By doing this, Scholte obtained good agreement between his assumed and calculated molecular weight distributions.

There are, however, three reasons why Scholte's scheme cannot be blindly applied to other systems. These are: (1) Scholte dealt with a molecular weight range of  $5 \times 10^4$  to  $10^6$ ; by comparison, in many cases of synthetic polymers the range is much narrower, e.g., 0 to  $10^5$ . (2) Scholte used five or more angular velocities, each requiring several days for equilibrium. There are, however, cases when equilibrium at each velocity requires a much longer time (Reference 8). Therefore, it is important to have a scheme which would produce a MWD from data taken at one velocity. (3) Since our interest was in a different molecular weight range and we were using experimental data from only one angular velocity, the effects of experimental error on the calculated MWD had to be investigated.

A computer program using Scholte's ideas was independently coded and a different linear programming (LP) solving routine was employed. The new program reliability was verified by reproducing Scholte's published results. Then application of the new program to new specific needs stated above were investigated. A brief description of linear programming theory follows.

## SECTION II

## THEORY

In the brief discussion which follows, all theorems and definitions are given without proof or examples. All material on linear programming was taken from other works (References 9, 10, and 11).

Definition 1. A simplex is an n-dimensional convex polyhedron having exactly  $n+1$  vertices. The boundary of the simplex contains simplicial faces of dimension  $i$  where  $i < n$ . The number of such faces of dimension  $i$  is  $\binom{n+1}{i+1}$  where  $\binom{n}{m} = n! / m!(n-m)!$ . A simplex in zero dimension is a point, in 1-dimension a line, in 2-dimension a triangle, in 3-dimension a tetrahedron, etc. The equation of a simplex with unit intercept is  $X_i \geq 0$  and  $\sum_i X_i = 1$ .

Definition 2. A subset  $C$  of  $E_n$  (n-dimensional Euclidean Space) is a convex set if and only if for all pairs of points  $V_1$  and  $V_2$  in  $C$  any convex combination

$$V = \beta_1 V_1 + \beta_2 V_2 \quad (1)$$

is also in  $C$ , where  $\beta_i$  are scalars,  $\beta_i \geq 0$ , and  $\sum_i \beta_i = 1$ .

Definition 3. A point  $V$  in a convex set  $C$  is called an extreme point if  $V$  cannot be expressed as a convex combination of any other two distinct points in  $C$ . That is, if we denote the convex set of solutions to the linear programming problem by  $K$  and if  $K$  is a convex polygon, then  $K$  is the convex hull of the extreme points of  $K$ . Therefore, every feasible solution in  $K$  can be represented as a convex combination of the extreme feasible solutions in  $K$ .

Theorem 1. The set of all feasible solutions to the linear programming problem is a convex set.

In general, the linear programming problem can be described as follows: Given is a convex set defined by a set of linear constraints in  $E_n$ . From all the points belonging to the convex set, we wish to determine a subset of points (which will contain either one or many points) for which a linear objective function is optimized.

Usually we are confronted with a set of simultaneous equations

$$\begin{array}{l} a_{11}x_1 + a_{12}x_2 + a_{13}x_3 + \cdots + a_{1m}x_m = b_1 \\ \vdots \qquad \qquad \qquad \qquad \qquad \qquad \qquad \vdots \\ a_{n1}x_1 + a_{n2}x_2 + a_{n3}x_3 + \cdots + a_{nm}x_m = b_n \end{array} \quad (2)$$

where  $n > m$ . For simplicity let  $m$  equal  $n$ ; let  $A$  be the matrix,  $\{a_{ij}\}$ , ( $i = 1, 2, 3, \dots, m$  and  $j = 1, 2, 3, \dots, m$ );  $X$  the vector  $[X_j]$ ,  $j = 1, 2, 3, \dots, m$  and  $b$  the vector  $\{b_i\}$ ,  $i = 1, 2, 3, \dots, m$ . Then Equation 2 can be written in the form

$$Ax = b \quad (3)$$

Since A is a square matrix and assumed nonsingular, the solution vector is expressed as

$$\underline{x} = A^{-1} \underline{b} \quad (4)$$

A simple computational scheme is the complete elimination method of Jordan and Gauss which has a finite number of steps or iterations. In just  $m$  iterations the procedure multiplies the system (Equation 2) by  $A^{-1}$  to obtain Equation 4. This is the standard matrix problem which is assumed familiar to the reader.

Now, in linear programming the problem is reversed. Instead of having an "over-determined" system as indicated by Equation 2, we have an "under-determined" system (i. e.,  $n < m$ ) subject to other constraints. That is, we wish to find a vector  $\{x_i\}$ ,  $i = 1, 2, 3, \dots, m$  which minimizes the linear form (i. e., the objective function)

$$C_1 x_1 + C_2 x_2 + C_3 x_3 + \dots + C_m x_m \quad (5)$$

subject to linear constraints

$$x_j \geq 0, \quad j = 1, 2, 3, \dots, m \quad (6)$$

and the set of equations given by Equation 2 but with  $n < m$ .

For large  $n$  and  $m$  it would be an impossible task to evaluate all possible solutions and select one that minimizes the objective function. A computational

scheme is desired which converges to a minimum solution. The Simplex Method, devised by Dantzig (Reference 11) is such a scheme. In Reference 11 the equation  $\sum X_i$  is used as a constraint. The procedure finds an extreme point and determines whether it is the minimum. If it is not, the procedure finds a neighboring extreme point whose corresponding value of the objective function is less than or equal to the preceding value. In a finite number of such steps (usually between  $n$  and  $2n$ ), a minimizing feasible solution is found. The Simplex Method makes it possible to discover whether the problem has any finite minimizing solutions or no feasible solutions at all.

Consideration is now given to how this can be related to the problem at hand, namely, molecular weight determination via sedimentation-diffusion equilibrium. The equation describing sedimentation-diffusion equilibrium for a heterogeneous system is given (from Reference 1) by

$$-\frac{1}{C^0} \frac{dC}{d\xi} = \int_0^\infty \frac{\lambda^2 M^2 e^{-\lambda M} F(M)}{1 - e^{-\lambda M}} dM \quad (7)$$

where,

$$\int_0^\infty F(M) dM = 1 \quad (8)$$

In the above equations  $C^0$  is the concentration of the original solution,  $C$  is the equilibrium concentration at radial distance  $r$ ,  $M$  is the molecular weight,  $F(M)$  is the frequency function of molecular weight,  $\xi = (r_b^2 - r^2)/(r_b^2 - r_m^2)$  with  $r_m$  the radial distance from the center of rotation to the meniscus, and  $r_b$  the radial distance from the center of rotation to the bottom of the cell. Also,  $\lambda = (1-v\rho) \omega^2 (r_b^2 - r_m^2)/2RT$ , where  $v$  is the partial specific volume of the dissolved substance,  $\rho$  is the density of the solution,  $\omega$  is the angular velocity in radian per second,  $R$  is the gas constant, and  $T$  the absolute temperature.

Rewriting Equations 7 and 8 for the discrete case (Dirac  $\delta$ -functions) one obtains

$$U(\lambda_i, \xi_n) = \sum_m \frac{\lambda_i^2 M_m^2 e^{-\lambda_i M_m \xi_n}}{1 - e^{-\lambda_i M_m}} f_m \quad (9)$$

and,

$$\sum_m f_m = 1 \quad (10)$$

where

$$U(\lambda_i, \xi_n) = - \frac{1}{C_0} \left( \frac{dC}{d\xi_n} \right) \lambda_i \quad \text{and} \quad f_m$$

is the weight fraction of molecules of a given molecular weight  $M_m$  in the original sample. Recall that the  $U(\lambda_i, \xi_n)$  and  $\xi_n$  are the experimentally measured quantities with  $\lambda_i$  being the product of a constant (determined from auxiliary measurements) and the square of the angular speed of the rotor.

For convenience of notation let

$$K_{\ell n} = \frac{\lambda_i^2 M_m^2 e^{-\lambda_i M_m \xi_n}}{1 - e^{-\lambda_i M_m}} \quad (11)$$

and

$$U_\ell = U(\lambda_i, \xi_n) \quad (12)$$

where for each  $i, n = 1, 2, \dots, N; i = 1, 2, \dots, I; m = 1, 2, \dots, M$ ; and  $\ell = 1, 2, \dots, L$  with  $L = IN$  and  $L > M$ .

Thus Equation 9 becomes

$$U_\ell = \sum_m K_{\ell m} f_m \quad (13)$$

Since the quantities of  $U_\ell$  are experimentally measured, they will in all probability be greater than or less than their true precise value (i.e., there exists experimental error). Although this physical fact is accepted, experimentally Equation 13 does not hold true. This is especially apparent when we investigate the matrix  $\{K_{\ell m}\}$  and find it ill-conditioned. In essence, the matrix  $\{K_{\ell m}\}^{-1}$  acts as an "amplifier" for any error which might exist in the set  $\{U_\ell\}$ .

If we grant that an error in  $U_\ell$  exists, Equation 13 becomes

$$U_\ell = \sum_m K_{\ell m} f_m + \epsilon_\ell \quad (14)$$

where  $\epsilon_\ell$  is the experimental error in  $U_\ell$ . Since the application of linear programming necessitates that all  $x_i$  (see Equation 1) are positive or zero, we must account for error's being positive or negative. It is the inclusion of error that now enables us to go from an "over determined" system to an "under determined" system. The linear programming procedure is now applicable. In particular, you will recall that a modified Simplex Method can be used.

Recapitulating, we now obtain the formulation of the linear programming scheme as used to determine the MWD from sedimentation-diffusion equilibrium. We wish to find the set  $\{f_m\}$ ,  $m = 1, 2, \dots, Q$ , which minimizes the linear form (i. e., the objective function)

$$\sum_{\ell=1}^L (\delta_\ell + \beta_\ell) \quad (15)$$

subject to the linear constraints

$$\begin{aligned} f_m &\geq 0, \quad m = 1, 2, 3, \dots, Q \\ \delta_\ell &\geq 0 \} , \ell = 1, 2, 3, \dots, L \\ \beta_\ell &\geq 0 \end{aligned} \quad (16)$$

and

$$\begin{aligned} K_{11}f_1 + K_{12}f_2 + \dots + K_{1Q}f_Q + \delta_1 - \beta_1 + 0 + 0 + \dots + 0 + 0 &= U_1 \\ K_{21}f_1 + K_{22}f_2 + \dots + K_{2Q}f_Q + 0 + 0 + \delta_2 - \beta_2 + \dots + 0 + 0 &= U_2 \\ \vdots & \\ K_{L1}f_1 + K_{L2}f_2 + \dots + K_{LQ}f_Q + 0 + 0 + 0 + \dots + \delta_L - \beta_L &= U_L \end{aligned} \quad (17)$$

where  $L > Q^{**}$ . Let the set  $\{x_i\}$ ,  $i = 1, 2, 3, \dots, Q + 2L$  be composed of  $f_m$  values for  $i = 1, 2, 3, \dots, Q$ , and alternately  $\delta_\ell$  and  $\beta_\ell$  for  $i = Q + 1, Q + 2, \dots, Q + 2L$ ; where all  $X_i \geq 0$ . Also let the  $L \times (Q + 2L)$  matrix  $P$  be represented by

---

\*\*This is not an absolutely necessary condition. When one velocity was used the situation arose where  $L < Q$ .

$$P = \begin{pmatrix} K_{11} & K_{12} & \cdots & K_{1Q} & 1 & -1 & 0 & 0 & \cdots & 0 & 0 \\ K_{21} & K_{22} & \cdots & K_{2Q} & 0 & 0 & 1 & -1 & \cdots & 0 & 0 \\ \vdots & & & \vdots & & & & & & \vdots & \\ K_{L1} & K_{L2} & \cdots & K_{LQ} & 0 & 0 & 0 & 0 & \cdots & 1 & -1 \end{pmatrix} \quad (18)$$

Then, in matrix notation the problem is formulated by

$$\underline{PX} = \underline{U} \quad (19)$$

The next section will describe the application of this method.

## SECTION III

VARIABLE FACTORS IN COMPUTATION AND  
THEIR INFLUENCE ON RESULTING MWD

## A. FORMULATION OF COMPUTER PROBLEM

The objective of this section is to present the results which three variable factors investigated have on a MWD. Since the actual programming involved a slight modification of Equation 9, a listing and discussion of the variable factors investigated will be preceded by a discussion of the actual equation programmed.

The programmed equation is given by

$$U(\lambda_k, \xi_i) = \sum_n \frac{\lambda_k^2 M_n^2 e^{-\lambda_k M_n \xi_i} F(M_n) \Delta M_n}{1 - e^{-\lambda_k M_n}} \quad (20)$$

Here all quantities have the same meaning as in Equation 7 and 9. However, we must remember that, since  $\lambda$  is proportional to the square of the angular velocity, the index  $k$  indicates the various velocities at which equilibrium was achieved. For each velocity there exists a set of  $\xi$ -values, i.e., for each  $\lambda_k$  there is a corresponding set  $\{\xi_i\}$ . If there are data from five velocities and for each velocity there corresponds five  $\xi$ -values, this would imply twenty-five  $U$ -values. It is imperative that the molecular weight range being investigated incorporate all molecular weights present in the solution sample being centrifugated. Since Equation 9 and 20 deal with discrete molecular weights, some procedure must be employed to span the entire molecular weight range (MWR). Following the idea of Scholte (References 6 and 7), a multiplicative factor (g-factor) has been introduced. Therefore, starting with the first molecular weight  $M_1$ , the other molecular weights in a given sampled set could be generated. Knowing, a priori, the MWR we can now calculate the g-factor and the number ( $N_Q$ ) of molecular weights needed to span the MWR. (The g-factor is later used as a variable parameter related to the error in the experimental concentration gradients. However, the value of g must be at least large enough to ensure the actual MWR present in a given experiment

is spanned. A convenient technique for finding the MWR is given in Reference 8). The molecular weights sampled will be

$$M_n = M_1 g^{n-1} \quad (21)$$

where  $n = 1, 2, 3, \dots, N_Q$ . This enables one to divide the MWR into non-overlapping subranges. Each subrange span is denoted by

$$\Delta M_n = M_n - M_{n-1} \quad (22)$$

where  $M_0$  is assumed zero. By employing the averaging technique of Scholte (Reference 7), after solving Equation 20 for one set of molecular weights, a new set of molecular weights is selected in a prescribed manner. The new set is shifted relative to the previous set by a multiplicative factor  $g^{1/N}$ , where  $N$  is the number of desired molecular weight sets. That is, if the number of the set is labeled by the index  $n$  and the molecular weights within a set by  $j$ , then

$$M_{j,n} = M_{1n} g^{j-1} \quad (23)$$

and

$$\Delta M_{jn} = (g^{1/2} - g^{-1/2}) M_{jn} \quad (24)$$

where  $j = 1, 2, 3, \dots, NQ$ ;  $n = 1, 2, 3, \dots, N$ ; and  $M_{0,n} = 0$ .

The concentration of molecular weights in a given subrange is simply the weight fraction ( $f_m$ ) multiplied by the initial solution concentration ( $C^{\circ}_m = C^{\circ}f_m$ ). When Scholte (Reference 7) presents his final results they are in the form  $MF(M)$  versus  $M$ . In this work a modified system  $F(M)$  versus  $M$  has been calculated (Equation 20), since one usually has less qualitative feeling for  $MF(M)$  than for  $F(M)$ .

Now, it is possible to list the variable parameters investigated in this work. They are as follows:

1. The effect that varying the  $g$ -factor (i. e., the span of the molecular weight subrange) has on the resulting MWD; and also the effect when the number of sets of molecular weights sampled was varied.

2. How the resulting MWD is affected by varying the number of elements in the sets  $\{\xi_i\}$  and  $\{\lambda_k\}$ .

3. Whether the introduction of error into idealized U-values affects the resulting MWD. This includes normal random error and weighted random error.

The results of each will be discussed successively in the following section.

#### B. DISTRIBUTIONS STUDIED

The g-factor is related to the experimental error in the U-values (Reference 7). Figures 1 through 4 show the effect of varying the g-factor and the number of sets of molecular weights. In each case the solid-line curve is the assumed distribution from which U-values were calculated. For all curves, seven velocities were used and with each velocity five  $\xi$ -values. The squared angular velocities were  $4.1693 \times 10^5$ ,  $5.8370 \times 10^5$ ,  $8.1718 \times 10^5$ ,  $11.4406 \times 10^5$ ,  $16.0168 \times 10^5$ ,  $22.4235 \times 10^5$ , and  $31.3929 \times 10^5 \text{ rad}^2/\text{sec}^2$  with  $\xi = 0, 1/4, 1/2, 3/4, \text{ and } 1$  for each case. Therefore, thirty-five U-values were used for these calculations.

As previously mentioned, we must always be sure that the MWR is wide enough to incorporate all molecular weights present in the sample. To study the effect of range size on the MWD, all parameters in Figure 4 were held constant except the value for MWR, which was brought closer to the MWR of the assumed distribution. As shown in Figure 5, structure begins to appear when the highest molecular weight sampled was not far beyond the actual highest molecular weight present. Figure 5 represents a calculation involving twenty molecular weight sets. When the number of molecular weight sets was decreased from twenty to ten (Figure 6) then five (Figure 7), there was no appreciable change except that, naturally, the calculated points were spaced farther apart.

What would be the effect if the number of  $\xi$ -values associated with each velocity was increased? As previously mentioned, five  $\xi$ -values have been used per velocity for Figures 1 through 7. Figure 8 shows the results with all

parameters of Figure 6 held constant except that, now, nine  $\xi$ -values were used. The nine  $\xi$ -values were so chosen that  $\xi = 0$  to 1 with  $\Delta \xi = 1/8$ . From the study of this assumed distribution it appears that using five  $\xi$ -values, sampling twenty sets of molecular weights, and using a g-factor  $\approx 2.0$  seemed to have produced the optimum desired results, i. e., the calculated MWD agreeing best with the assumed MWD. If the g-factor became too small the result was noise, that is, the accuracy of the U-values did not warrant such precision, or the matrix in the LP solver routine became singular.

At this stage a normal Gaussian distribution with a MWR of 0 to 120,000 was investigated. Once again the g-factor was varied. The lowest g-value used was 1.15 and the highest 4.0. The former resulted in an erratic MWD and the latter resulted in a curve which went exponentially to zero at high molecular weights. The best g-value for this specific case was  $g = 1.8$ . In general, a satisfactory technique was to start with a low value of  $g$ . Then as the value of  $g$  was increased the erratic behavior of the MWD disappeared. At the g-value where the erratic results seemed to disappear, that value was established as the appropriate one. Then the maximum reliable "fine structure" for a given set of experimental U-values was attained.

Using this assumed normal distribution (its functional form) the MWR was shifted to investigate the reliability of the method for various molecular weight ranges. One range tried was from 0 to 12,000 and another from  $10^5$  to  $10^6$ . In each case the results were satisfactory, considering that in all cases  $g$  was kept constant ( $g = 1.8$ ).

As previously mentioned, the U-values used resulted from seven assumed velocities ranging from about 6,000 to 50,000 RPM. It would be advantageous if the experimental U's were obtained from an equilibrium sedimentation-diffusion experiment at only one angular velocity. To check this, the normal Gaussian distribution, MWR from 0 to 120,000, was approximated (holding all other variables constant) by deleting all U-values associated with various angular velocities. All combinations of the velocities were tried. By using only the lowest angular velocity (6,166 RPM), the computer program produced a MWD which "fit" the assumed MWD as well as the case where all seven angular velocities were used. In fact, all single velocity cases resulted in

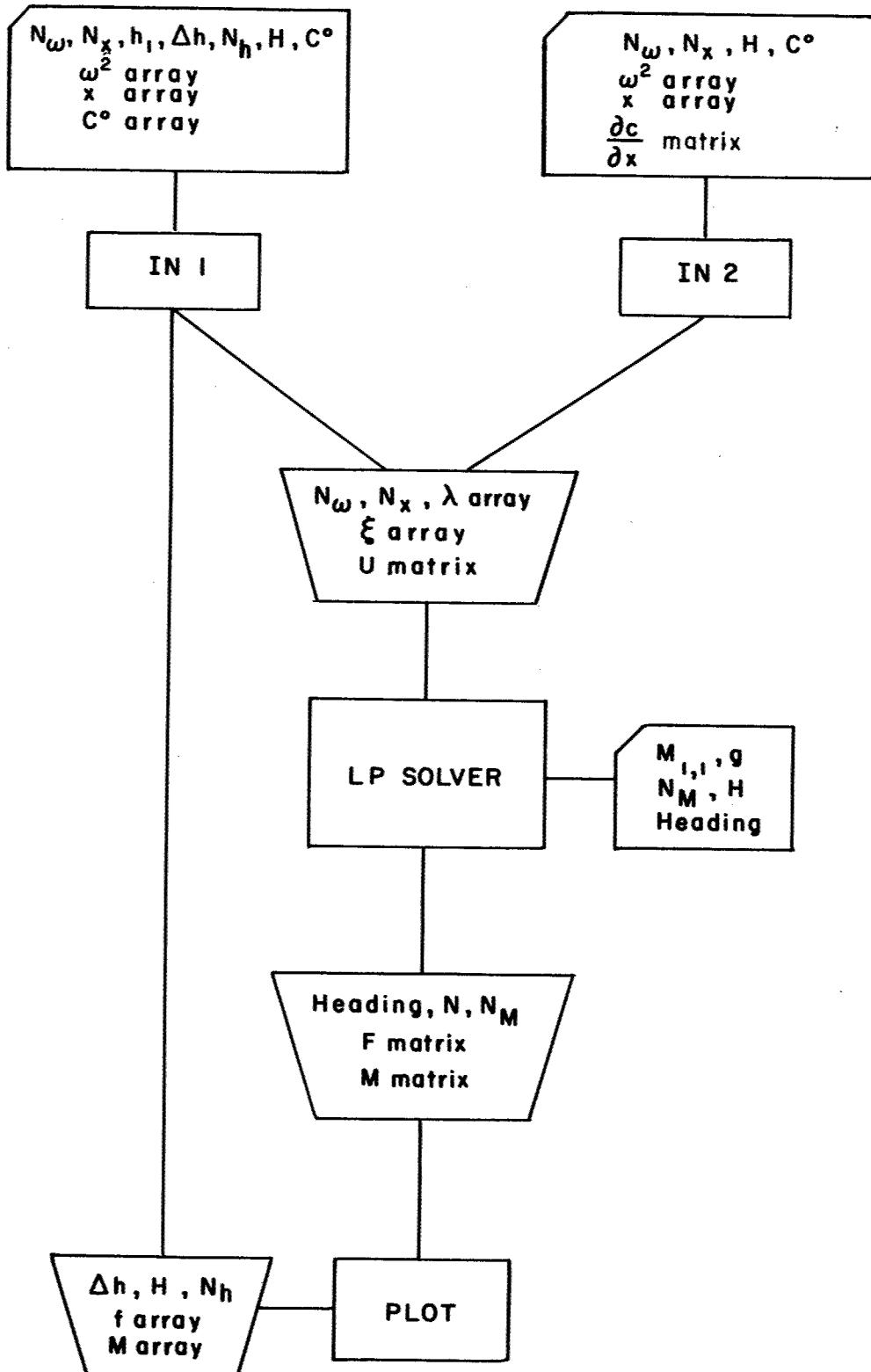
## PART III

a reasonable MWD. Therefore, we would conclude that an acceptable MWD could be obtained from an equilibrium sedimentation-diffusion experiment at one angular velocity, at least with a MWR of 0 to 120,000.

The third area of investigation involved use of the normal Gaussian MWD ( $0 < M < 120,000$ ) U-values from one angular velocity (6,166 RPM) and at  $\xi = 0, 1/4, 1/2, 3/4$ , and 1 to find the effect that error in the U-values would have on the calculated MWD. Error (1, 2, 5, 10, and 20%, respectively) was introduced by aid of a random error generator. For each magnitude of error, five calculations were employed to vitiate any wrong conclusions that one error distribution might have on the final MWD. For each case (1 to 20%) when the error was normally distributed (dotted line Figure 9) the calculated MWD agreed with the assumed MWD. Naturally the 1% error case gave the best "fit" to the assumed MWD, but even for the 20% error case the calculated MWD was not unacceptable. When the error introduced in the U-values was such as to be weighted (dashed curves Figure 9), the calculated MWD was entirely different from the expected normal MWD. This phenomenon substantiates the findings of Lee (Reference 5) and Tikhonov and Glasko (Reference 12).

SECTION IV  
DESCRIPTION OF COMPUTER PROGRAM

FLOW DIAGRAM



## DESCRIPTION OF VARIABLES

$a_{i,j}$	- entry in matrix for LP problem
$b$	- largest $x$ value
$b_i$	- right-hand side of LP problem
$C^\circ$	- initial concentration of solution
$C_m^\circ$	- initial concentration of solution whose molecular weight is $\frac{h}{H}$
$f_n$	- weight fraction of molecular weight $M_n$
$F_{j,n}$	- results of LP solution, frequency list for mol. wt. of $M_{j,n}$
$g$	- M multiplier
$h_n$	- input test array which is a function of molecular weight (References 5 and 8)
$H$	= $\frac{2RT}{1-v\rho}$
$m$	- smallest $x$ value
$M_n$	- molecular weight array associated with input test array
$M_{j,n}$	- molecular weight matrix of values used in LP solution
$N$	- number of LP sets to try
$N_h$	- number of input $h$ values
$N$	- number of $M$ values to use for use LP solution
$N_\omega$	- number of input $\omega^2$ values
$N_x$	- number of input $x$ values
$U_{k,l}$	= - $\frac{1}{C^\circ} \frac{dc}{d\xi}$
$x_l$	- array of distances squared from center of rotation
$\lambda_k$	- function of $\omega^2_k$
$\Delta h$	- constant difference between values of $h_n$ array
$\Delta M_{j,n}$	- difference between successive $j$ values of $M_{j,n}$ matrix
$\xi_l$	- function of $x_l$
$\omega^2$	- square of the angular velocity

## IN 1 ROUTINE

Input:  $N_\omega$ ,  $N_x$ ,  $h_1$ ,  $\Delta h$ ,  $N_h$ ,  $H$ ,  $C^\circ$ ,  $\omega_k^2$  array, where  $k = 1, \dots, N_\omega$   
 $x_j$  array, where  $\ell = 1, \dots, N_x$   
 $C^\circ_n$  array, where  $n = 1, \dots, N_h$

1.  $h_{n+1} = h_n + \Delta h$  for  $n = 1, \dots, (N_h - 1)$

2.  $m = x_1$

$$b = x_{N_x}$$

$$\lambda_k = (b-m) \cdot H \cdot \omega_k^2 \text{ for } k = 1, \dots, N_\omega$$

3.  $\xi_\ell = \frac{b-x_1}{b-m}$  for  $\ell = 1, \dots, N_x$

4.  $M_n = \frac{h_n}{H}$  for  $n = 1, \dots, N_h$

$$f_n = \frac{C^\circ_n}{C^\circ}$$

5.  $U_{k,\ell} = \sum_{n=1}^{N_h} \frac{(\lambda_k M_n)^2 e^{-\lambda_k M_n \xi_\ell}}{1 - e^{-\lambda_k M_n}} f_n$

for  $k = 1, \dots, N_\omega$  and  $\ell = 1, \dots, N_x$

6. Write out  $\omega^2$  array,  $\xi$  array, and  $U$  matrix

7. Call LP SOLVER

## IN 2 ROUTINE

Input:  $N_{\omega}$ ,  $N_x$ ,  $H$ ,  $C^\circ$ ,  $\omega_k^2$  array where  $k = 1, \dots, N_{\omega}$

$x_\ell$  array where  $\ell = 1, \dots, N_x$

$(\frac{dC}{dx})_{k\ell}$  matrix where  $k = 1, \dots, N_{\omega}$  and  
 $\ell = 1, \dots, N_x$

1.  $m = x_1$

$b = x_{n_x}$

2.  $\lambda_k = (b-m) H \omega_k^2$  for  $k = 1, \dots, N_{\omega}$

3.  $\xi_\ell = \frac{b-x_\ell}{b-m}$  for  $\ell = 1, \dots, N_x$

4.  $U_{k,\ell} = \frac{b-m}{C^\circ} (\frac{dc}{dx})_{k,\ell}$  for  $k = 1, \dots, N_{\omega}$   
 and  $\ell = 1, \dots, N_x$

5. Write out  $\omega^2$  array,  $\xi$  array, and U matrix

6. Call LP SOLVER

## LP SOLVER

1. Input from IN 1:  $N_{\omega}$ ,  $N_x$ ,  $\lambda$  array,  $\xi$  array, and U matrix

2. Input from cards:  $M_{1,1}$ , g,  $N_M$ , N, HEADING

3. Write out input from cards

4.  $N_{\text{row}} N_{\omega} : N_x$

$$N_{\text{col}} = N_M + 2 N_{\text{row}}$$

$$n = 1$$

5. Calculate the following matrix entries

$$a_{i,j} = 1 \text{ for } i = 1, \dots, N_{\text{row}} \text{ and } j = N_M + 1, N_{\text{col}-1}, 2$$

$$a_{i,j} = 1 \text{ for } i = 1, \dots, N_{\text{row}} \text{ and } j = N_M + 1, N_{\text{col}}, 2$$

$$a_{i,j} = \frac{(\lambda_k M_{j,n})^2 e^{-\lambda_k M_{j,n}}}{1 - e^{-\lambda_k M_{j,n}}} \Delta M_{j,n}$$

$$\text{for } i = 1, \dots, N_{\text{row}} \text{ and } j = 1, \dots, N_M$$

$$\text{where } k = \left[ \frac{i-1}{N_x} \right] + 1$$

$$\ell = i(k-1) \cdot N_x$$

$$M_{j,n} = M_{1,n} \cdot g^{j-1}$$

and

$$\Delta M_{j,n} = (g^{1/2} - g^{-1/2}) M_{j,n}$$

6. Calculate the following right-hand sides  $b_i = U_{k,\ell}$  where  $i, k$ , and  $\ell$  are defined as in step 5.

7. Calculate the following objective coefficients

$$C_j = 0 \text{ for } j = 1, \dots, N_M$$

$$C_j = 1 \text{ for } j = N_M + 1, \dots, N_{\text{col}}$$

## LP SOLVER

8. Write out the determinants of:

$$\begin{bmatrix} a_{i,j} \end{bmatrix} \text{ for } i = 1, \dots, N_M \text{ and } j = 1, \dots, N_M$$

$$\begin{bmatrix} a_{i,j} \end{bmatrix} \text{ for } i = N_M + 1, \dots, 2 \cdot N_M$$

$$\begin{bmatrix} a_{i,j} \end{bmatrix} \text{ for all sets of } N_M \text{ rows less than } N_{\text{row}}$$

9. Write out matrix  $\begin{bmatrix} a_{i,j} \end{bmatrix}$  for  $i = 1, \dots, N_{\text{row}}$  and  $j = 1, \dots, N_M$  in exponent form.

10. Call LP solver and store solutions in  $F_{j,n}$  array.

11. Write out    input RHS  
                   computer RHS using solution  
                   difference of RHS'S  
                   absolute value of relative differences of RHS  
                   average absolute relative difference

12.  $n \leftarrow n + 1$

$$M_{1,n} \leftarrow (M_{1,n-1})g^{1/N}$$

13. Return to step 5 until n exceeds N

14. Write out  $F_{j,n}$  matrix

15. Call PLOT routine

## PLOT ROUTINE

1. Input from LP SOLVER: HEADING, N,  $N_m$ , F, and M matrices
2. Input from IN 1 (if used):  $\Delta h$ , H,  $N_n$ , f, and M arrays
3.  $\Delta M = \frac{\Delta h}{H}$
4. Write out heading
5. Label vertical axis F(M)
6. Label horizontal axis M
7. Plot  $\frac{f_n}{\Delta M}$  versus  $M_n$  for  $n = 1, \dots, N_h$
8. Plot  $F_{j,n}$  versus  $M_{j,n}$  for  $n = 1, \dots, N$  and  $j = 1, \dots, N_M$
9. STOP

## SECTION V

## CONCLUSION

To date, the linear programming method seems to be one of the most promising schemes for obtaining the molecular weight distribution from sedimentation-diffusion equilibrium data. There are five main features of this investigation which are worthy of mention.

1. The linear programming method has been found to give acceptable results for the case of experimental data obtained at one angular velocity.
2. It was found that if a normal random error of the experimental gradient curve was about 20% the linear programming method produced a MWD with satisfactory precision. However, if the experimental error was weighted, i. e., the concentration gradient curve was distorted from the true curve, a 1 or 2% error led to an absurd molecular weight distribution. This agrees with the findings of Lee (Reference 5), Tikhonov and Glasko (Reference 12), and Tikhonov (References 13 and 14).
3. This investigation did not involve any modification of the LP solver routine. The LP solver limitations were manifested by spurious points sometimes appearing in the determined molecular weight distribution. In general, the linear programming method presents only an overall molecular weight structure. Therefore, when twenty sets of molecular weights were sampled, it was obvious when one point was completely illogical.
4. A great improvement was achieved by solving for  $F(M)$  directly (Equation 20), rather than via  $f_m$  (Equation 9). In the former case the matrix presented to the LP solver routine was not so ill-conditioned (Tables I and II).
5. The following test was made after each call of the LP solver routine. By having the calculated MWD, the computer program could calculate new  $U$ -values ( $U_{\text{calc}}$ ). The difference between  $U_{\text{exp}}$  and  $U_{\text{calc}}$  was then printed. Also, the absolute relative differences, the averaged absolute relative error for one set of molecular weights, and the averaged absolute relative error averaged over all molecular weight sets were printed. In general, a good "fit" between the assumed MWD and the derived MWD showed low values for

all the above error analyses; however, the converse was not always found to hold true. At present much effort is being focused on determination of a procedure for obtaining a one-to-one correspondence between the error analysis criteria and the "fit" of the derived MWD.

TABLE I  
EXPONENTS OF ELEMENTS IN THE MATRIX PRESENTED TO  
LP SOLVER ROUTINE USING EQUATION 9\*

-2	-1	-1	-1	0	0	0	0	0	0
-2	-1	-1	-1	0	0	0	0	0	0
-2	-1	-1	-1	0	0	0	0	0	0
-2	-1	-1	-1	0	0	0	0	0	0
-2	-1	-1	-1	0	0	0	0	0	1
-1	-1	0	0	0	0	0	0	-2	-5
-1	-1	0	0	0	0	0	0	-1	-3
-1	-1	0	0	0	0	0	0	0	-1
-1	-1	0	0	0	0	0	0	0	0
-1	-1	0	0	0	0	0	1	1	2

\* Value of determinant = - 0.3932972 E - 31

TABLE II  
EXPONENTS OF ELEMENTS IN THE MATRIX PRESENTED TO  
LP SOLVER ROUTINE USING EQUATION 20\*

1	1	2	3	3	4	4	5	5	5
1	1	2	3	3	4	4	5	5	5
1	1	2	3	3	4	4	5	6	6
1	1	2	3	3	4	5	5	6	6
1	1	2	3	3	4	5	5	6	7
1	2	3	3	4	4	4	4	3	0
1	2	3	3	4	4	5	5	4	2
1	2	3	3	4	4	5	5	5	4
1	2	3	3	4	5	5	6	6	6
1	2	3	3	4	5	5	6	7	8

\* Value of determinant = - 0.1500715 E 17

**APPENDIX**

**LISTING OF COMPUTER PROGRAM**

AFML-TR-67-121  
PART III

```
*$BFTC EXEC. DECK          FXFC.001
C                                         EXEC.002
C      MAIN PROGRAM EXECUTIVE CONTROL      FXFC.003
C      INITIALIZE PLOTTING ROUTINS        EXEC.004
C      INITIALIZE PLOT COUNT             EXEC.005
C      DETERMINE SEQUENCE OF SUBROUTINES CALLED EXEC.006
C      TERMINATE PLOTTING BEFORE EXITING   EXEC.007
C      WRITE HEADING AND PLOT COUNT       EXEC.008
C                                         EXEC.009
C      COMMON /PLTR/ PDATA(438), IPLTS, HEAD(12) EXEC.010
C      COMMON /PRTCTL/ WRITE               EXEC.011
C                                         EXEC.012
C      LOGICAL WRITE                     EXEC.013
C                                         EXEC.014
C      IPLTS = 0                         EXEC.015
C      CALL PLOTS ( PDATA, 438 )          EXEC.016
1 READ (5,500) HEAD                  EXEC.017
      WRITE (6,600) HEAD                EXEC.018
      CALL INI ( $900 )                 EXEC.019
      IF ( WRITE ) WRITE (6,600) HEAD    EXEC.020
      CALL LPS ( $900 )                 EXEC.021
      CALL PLOTR                      EXEC.022
      GO TO 1                         EXEC.023
900 WRITE (6,601) IPLTS            EXEC.024
      CALL PLOTE                      EXEC.025
      STOP                           FXFC.026
500 FORMAT ( 12A6 )                 EXEC.027
600 FORMAT ( 1H1, 12A6 / ( 1X, 12A6 ) ) EXEC.028
601 FORMAT ( 1H0, I2, 17H PLOT(S) COMPLETE ) EXEC.029
      END                           EXEC.030
```

```
$IBFTC BIN1. DECK                                BIN1.001
C                                                 BIN1.002
C   BLOCK DATA SUBPROGRAM TO SUPPLY INPUT DATA WHEN INP1. IS BY-PASSED BIN1.003
C                                                 BIN1.004
C   BLOCK DATA                                     BIN1.005
C                                                 BIN1.006
C   COMMON /BIN1/ NW, NX, XL(20), Z(20), U(20,20)    BIN1.007
C                                                 BIN1.008
C   DATA NW /5/
C   DATA NX /5/
C   DATA XL / 2.5E-6, 10.E-6, 40.E-6, 160.E-6, 640.E-6, 15*0. /
C   DATA Z /1.0, .75, .5, .25, 0., 15*0. /
C   DATA U / .187, .405, .372, .144, .005,           15*0.,,
C          .208, .554, .639, .337, .026,             15*0.,,
C          .232, .799, 1.346, .959, .164,             15*0.,,
C          .260, 1.237, 0., 0., 0., ,                 15*0.,,
C          .294, 2.121, 0., 0., 0., ,                 15*0.,,
C  X 300*0. /
C  END                                              BIN1.019
```

```
*1RETC BDR.  
      BLOCK DATA  
C      X IS R**2  
C  
      COMMON /BLOCKR/ X(20)  
      DATA X / 36.548312,  
           X      39.358308,  
           X      42.272363,  
           X      46.838556,  
           X      48.412651,  
           X      50.012759,  
           X      14*0.    /  
      END  
BDR.0001  
BDR.0002  
BDR.0003  
BDR.0004  
BDR.0005  
BDR.0006  
BDR.0007  
BDR.0008  
BDR.0009  
BDR.0010  
BDR.0011  
BDR.0012  
BDR.0013
```

```
$IRFTC BD.      DECK          BD.00001
^
^  BLOCK DATA SUBPROGRAM FOR 122 CO VALUES AND 7 W2 VALUES   BD.00002
^
^  BLOCK DATA          BD.00003
^
^  COMMON /BLOCKW/ W2(20)          BD.00004
^  COMMON /BLOCKC/ CO(160)          BD.00005
^
^  DATA W2          BD.00006
1/416930.0, 583702.0, 817182.8, 1144056., 1601678., 2242349.,
22139289., 13*0.    /
^
^  DATA CO          BD.00007
1 .170E-5, .350E-5, .530E-4, .115E-3, .850E-4, .550E-4, .310E-4, BD.00008
2 .750E-5, .700E-5, .650E-5, .820E-5, .100E-4, .135E-4, .170E-4, BD.00009
3 .260E-4, .340E-4, .360E-4, .370E-4, .300E-4, .225E-4, .215E-4, BD.00010
4 .205E-4, .301E-4, .400E-4, .435E-4, .470E-4, .410E-4, .350E-4, BD.00011
5 .280E-4, .210E-4, .225E-4, .235E-4, .245E-4, .260E-4, .258E-4, BD.00012
6 .255E-4, .245E-4, .235E-4, .225E-4, .210E-4, .205E-4, .200E-4, BD.00013
7 .310E-4, .420E-4, .440E-4, .420E-4, .380E-4, .340E-4, .300E-4, BD.00014
8 .260E-4, .255E-4, .250E-4, .245E-4, .240E-4, .232E-4, .225E-4, BD.00015
9 .215E-4, .205E-4, .190E-4, .170E-4, .163E-4, .155E-4, .175E-4, BD.00016
X .190E-4, .225E-4, .260E-4, .240E-4, .220E-4, .195E-4, .190E-4, BD.00017
1 .182E-4, .175E-4, .170E-4, .165E-4, .160E-4, .150E-4, .140E-4, BD.00018
2 .130E-4, .110E-4, .900E-5, .650E-5, .450E-5, .500E-5, .550E-5, BD.00019
3 .820E-5, .110E-4, .113E-4, .115E-4, .920E-5, .700E-5, .600E-5, BD.00020
4 .500E-5, .400E-5, .300E-5, .230E-5, .150E-5, .100E-5, .150E-5, BD.00021
5 .220E-5, .300E-5, .400E-5, .500E-5, .470E-5, .450E-5, .420E-5, BD.00022
6 .400E-5, .500E-5, .600E-5, .680E-5, .750E-5, .700E-5, .650E-5, BD.00023
7 .580E-5, .500E-5, .420E-5, .350E-5, .300E-5, .200E-5, .150E-5, BD.00024
8 .100E-5, .500E-6, .0, .0., .0., .36*0.    /
FND          BD.00025
^
^
```

```

*IBETC BD.      DECK          BD.00001
*                                BD.00002
*      BLOCK DATA SUBPROGRAM FOR 160 CO VALUES AND 7 W2 VALUES   BD.00003
*                                BD.00004
*      BLOCK DATA          BD.00005
*                                BD.00006
*      COMMON /BLOCKW/ W2(20)          BD.00007
*      COMMON /BLOCKC/ CO(160)         BD.00008
*                                BD.00009
*      DATA W2                  BD.00010
1/416930.0, 583702.0, 817182.8, 1144056., 1601678., 2242349.,
23139289., 13*0.    /
*                                BD.00011
*                                BD.00012
*                                BD.00013
*      DATA (CO(I),I=1,114)        BD.00014
1/.65000E-5,.00000E-5,.11000E-4,.13250E-4,.16000E-4,.19250E-4, BD.00015
2 .23250E-4,.28000E-4,.33500E-4,.40000E-4,.47750E-4,.56750E-4, BD.00016
3 .67250E-4,.79500E-4,.93750E-4,.11025E-3,.12925E-3,.15150E-3, BD.00017
4 .17700E-3,.20600E-3,.23925E-3,.27725E-3,.32050E-3,.36975E-3, BD.00018
5 .42525E-3,.48775E-3,.55825E-3,.63725E-3,.72575E-3,.82450E-3, BD.00019
6 .93425E-3,.105575E-2,.119025E-2,.133875E-2,.150175E-2,.168025E-2,BD.00020
7 .18755E-2,.208825E-2,.231925E-2,.256950E-2,.283950E-2,.313025E-2,BD.00021
8 .34420E-2,.377525E-2,.413075E-2,.450825E-2,.490775E-2,.532950E-2,BD.00022
9 .577325E-2,.623825E-2,.672375E-2,.722900E-2,.775275E-2,.829375E-2,BD.00023
X .885050E-2,.942100E-2,.01000325 ..01059475 ..01119325 ..01179625 ,BD.00024
1.01240075 ..01300375 ..01360175 ..01419175 ..01477075 ..01533475 ,BD.00025
2.01588050 ..01640475 ..01690400 ..01737525 ..01781500 ..01822000 ,BD.00026
3.01858775 ..01891575 ..01920150 ..01944275 ..01963800 ..01978575 ,BD.00027
4.01988475 ..01993450 ..01993450 ..01988475 ..01978575 ..01963800 ,BD.00028
5.01944275 ..01920150 ..01891575 ..01858775 ..01822000 ..01781500 ,BD.00029
6.01737525 ..01690400 ..01640475 ..01588050 ..01533475 ..01477075 ,BD.00030
7.01419175 ..01360175 ..01300375 ..01240075 ..01179625 ..01119325 ,BD.00031
8.01059475 ..01000325 ..00942010 ..00885050 ..00829375 ..00775275 ,BD.00032
9.00722900 ..00672375 ..00623825 ..00577325 ..00532950 ..00490775 /BD.00033
*      DATA (CO(I),I=115,160)        BD.00034
1/.00450825,.00413075 ..00377525 ..00344200 ..00313025 ..00283950 ,BD.00035
2.002569500,.00231925 ..00208825 ..00187550 ..00168025 ..00150175 ,BD.00036
3.001338750,.00119025 ..00105575 ..034250E-3,.824500E-3,.725750E-3,BD.00037
4.637250E-3,.558250E-3,.487750E-3,.425250E-3,.369750E-3,.320050E-3,BD.00038
5.277250E-3,.239250E-3,.206000E-3,.177000E-3,.151500E-3,.129250E-3,BD.00039
6.110250E-3,.937500E-4,.795000E-4,.672500E-4,.567500E-4,.477500E-4,BD.00040
7.400000E-4,.335000E-4,.280000E-4,.232500E-4,.192500E-4,.160000E-4,BD.00041
8.132500E-4,.110000E-4,.900000E-5,.650000E-5 /BD.00042
*END                         BD.00043

```

```
$1BFTC BD.      DECK          BD.00001
C      BLOCK DATA SURPROGRAM FOR 32 CO VALUES AND 7 W2 VALUES    BD.00002
C      BLOCK DATA          BD.00003
C      COMMON /BLOCKW/ W2(20)          BD.00004
C      COMMON /BLOCKC/ CO(160)          BD.00005
C      DATA W2          BD.00006
1/416930.0, 583702.0, 817182.8, 1144056., 1601678., 2242349.,   BD.00007
23139289., 13*0. /          BD.00008
C      DATA CO          BD.00009
1/.9132400E-3, .3044140E-2, .6392700E-2, .1053272E-1, .1497716E-1  BD.00010
2,.2051750F-1, .2538812F-1, .3031964E-1, .3494672E-1, .3975646E-1  BD.00011
3,.4383562E-1, .4706240E-1, .4968036E-1, .5144596E-1, .5296804E-1  BD.00012
4,.5382040F-1, .5461188F-1, .5467276E-1, .5418570F-1, .5333334E-1  BD.00013
5,.5144596E-1, .4858448E-1, .4407914E-1, .3835616E-1, .3117200E-1  BD.00014
6,.2496194F-1, .1960426E-1, .1503806E-1, .1120244E-1, .7427700E-2  BD.00015
7,.4322599E-2, .8140020E-4, 128*0. /          BD.00016
      FND          BD.00017
                                BD.00018
                                BD.00019
                                BD.00020
                                BD.00021
                                BD.00022
```

\$IBMAP RAND.	100,DECK	RAND.001	
*	GENERATES UNIFORM RANDOM NUMBERS	RAND.002	
*	R=FLRAN(Y), Y DUMMY GIVES REAL NUMBER	RAND.003	
*	CALL SAVF(Z) GIVES LAST OCTAL VALUE	RAND.004	
*	CALL VALUE(Z) GIVES STARTING OCTAL VALUE	RAND.005	
FLRAN	FTRY	FLRAN	RAND.006
LDQ	FTRY	SAVE	RAND.007
MPY	FTRY	VALUE	RAND.008
STO	LDQ	RANDOM	RAND.009
CLA	MPY	GENERA	RAND.010
LGL	STO	RANDOM	RAND.011
FAD	CLA	AAA	RAND.012
TRA	LGL	28	RAND.013
VALUF	FAD	AAA	RAND.014
CLA*	TRA	1,4	RAND.015
STO	VALUF	3,4	RAND.016
TRA	CLA*	RANDOM	RAND.017
SAVE	STO*	1,4	RAND.018
CLA	TRA	RANDOM	RAND.019
STO*	1,4	3,4	RAND.020
TRA	1,4	1,4	RAND.021
RANDOM	OCT	343277244615	RAND.022
AAA	OCT	172000000100	RAND.023
GENERA	OCT	343277244615	RAND.024
FEND			RAND.025

```
*TRETC PLOTR. DECK
  SUBROUTINE PLOTR
    COMMON SCH(4), SCF(4)
    COMMON /PLTR/ PDATA(438), IPLTS, HEAD(12)
    COMMON /BINP1/ DH, H, NC, F(162), CM(162), SKIP2
    COMMON /BLPS/ N, NM, BF(1000), BM(1000), K
    COMMON /BIN2/ USEIN2
    DATA HTITLE /1HM/, FTITLE /4HF(M)/
    LOGICAL SKIP2
    LOGICAL USEIN2
    IF ( SKIP2 ) RETURN
    IF ( .NOT. USEIN2 ) GO TO 7
    SCH(1) = BM(1)
    SCH(2) = BM(K)
    GO TO 8
7   DM = DH/H
    DO 5 I = 1,NC
5   F(I) = F(I) / DM
    SCH(1) = AMIN1( CM(1), BM(1) )
    SCH(2) = AMAX1( CM(NC), BM(K) )
8   SCF(1) = 0.
    SCF(2) = 0.
    IF ( USEIN2 ) GO TO 15
    DO 10 I = 1,NC
10  SCF(2) = AMAX1( SCF(2), F(I) )
15  DO 20 I = 1,K
20  SCF(2) = AMAX1( SCF(2), BF(I) )
    CALL SCALE ( SCH, 15., 2, 1, 10. )
    CALL SCALE ( SCF, 10., 2, 1, 10. )
    IF ( USEIN2 ) GO TO 25
    CM(NC+1) = SCH(3)
    CM(NC+2) = SCH(4)
    F(NC+1) = SCF(3)
    F(NC+2) = SCF(4)
25  RM(K+1) = SCH(3)
    RM(K+2) = SCH(4)
    RF(K+1) = SCF(3)
    RF(K+2) = SCF(4)
    CALL PLOT ( 5., -11., -3 )
    CALL PLOT ( 0., .5, -3 )
    CALL AXIS ( 0., 0., HTITLE, -1, 16., 0., SCH(3), SCH(4), 10. )
    CALL AXIS ( 0., 0., FTITLE, 4, 10., 90., SCF(3), SCF(4), 10. )
    CALL SYMBOL ( 1., 9.5, .25, HEAD, 0., 72 )
    IF ( .NOT. USEIN2 ) CALL LINE ( CM, F, NC, 1, 0, 0 )
    CALL LINE ( RM, BF, K, 1, 1, 1 )
    CALL PLOT ( 15., 0., -3 )
    IPLTS = IPLTS + 1
    RETURN
  END
```

PLOTR.01  
PLOTR.02  
PLOTR.03  
PLOTR.04  
PLOTR.05  
PLOTR.06  
PLOTR.07  
PLOTR.08  
PLOTR.09  
PLOTR.10  
PLOTR.11  
PLOTR.12  
PLOTR.13  
PLOTR.14  
PLOTR.15  
PLOTR.16  
PLOTR.17  
PLOTR.18  
PLOTR.19  
PLOTR.20  
PLOTR.21  
PLOTR.22  
PLOTR.23  
PLOTR.24  
PLOTR.25  
PLOTR.26  
PLOTR.27  
PLOTR.28  
PLOTR.29  
PLOTR.30  
PLOTR.31  
PLOTR.32  
PLOTR.33  
PLOTR.34  
PLOTR.35  
PLOTR.36  
PLOTR.37  
PLOTR.38  
PLOTR.39  
PLOTR.40  
PLOTR.41  
PLOTR.42  
PLOTR.43  
PLOTR.44  
PLOTR.45  
PLOTR.46  
PLOTR.47  
PLOTR.48  
PLOTR.49

```

$IRETC ORDER. DECK
      SUBROUTINE ORDER ( X, Y, NM, N, K )
      COMMON /PRTCTL/ WRITE
      DIMENSION X(1), Y(1)
      LOGICAL WRITE
      J = 0
      DO 10 LN = 1,N
      N20 = (LN-1) * 20
      I = N20 + 1
      J = J + 1
      X(J) = X(L)
      Y(J) = Y(L)
      DO 10 I = 2,NM
      L = N20 + I
      J = J + 1
      X(J) = X(L)
      10 Y(J) = Y(L)
      K = J
      20 TEST = 0.
      DO 30 I = 2,J
      IF ( X(I-1) .LE. X(I) ) GO TO 30
      XS = X(I-1)
      YS = Y(I-1)
      X(I-1) = X(I)
      Y(I-1) = Y(I)
      X(I) = XS
      Y(I) = YS
      TEST = 1.
      30 CONTINUE
      IF ( (TEST .EQ. 0.) .OR. ( J .EQ. 2 ) ) GO TO 40
      J = J - 1
      GO TO 20
      40 IF ( WRITE ). WRITE (6,600) (I, X(I), Y(I), I=1,K)
      RETURN
      600 FORMAT ( 1H1, 15X, 1HM, 19X, 1HF / 1H /
                  ( 1X, I3, 2E20.7 ) )
      X
      END

```

ORDER.01  
ORDER.02  
ORDER.03  
ORDER.04  
ORDER.05  
ORDER.06  
ORDER.07  
ORDER.08  
ORDFR.09  
ORDER.10  
ORDER.11  
ORDER.12  
ORDER.13  
ORDER.14  
ORDER.15  
ORDER.16  
ORDER.17  
ORDER.18  
ORDFR.19  
ORDFR.20  
ORDER.21  
ORDER.22  
ORDER.23  
ORDER.24  
ORDER.25  
ORDER.26  
ORDER.27  
ORDER.28  
ORDER.29  
ORDER.30  
ORDER.31  
ORDER.32  
ORDER.33  
ORDFR.34  
ORDER.35  
ORDER.36  
ORDER.37

```
$IBFTC DETA. DECK
  SUBROUTINE DETA ( A, B, NM, NROW )
    COMMON /PRTCTL/ WRITE
    DIMENSION A(51,120), B(NM,NM)
    LOGICAL WRITE
    IF ( WRITE ) WRITE (6,600)
    J = 1
10  DO 20 I = 1,NM
    DO 20 K = 1,NM
    JI = J + I
20  B(I,K) = A(JI,K)
    D = DET ( B, NM )
    IF ( WRITE ) WRITE (6,601) J, D
    J = J + NM
    IF ( (J+NM-1) .GT. NROW ) RETURN
    GO TO 10
600 FORMAT ( 13H0DETERMINANTS )
601 FORMAT ( 3X, 14, E19.7 )
END
```

DETA.001  
DETA.002  
DETA.003  
DETA.004  
DETA.005  
DFTA.006  
DETA.007  
DETA.008  
DETA.009  
DETA.010  
DETA.011  
DETA.012  
DETA.013  
DETA.014  
DETA.015  
DETA.016  
DETA.017  
DETA.018  
DFTA.019

```

$IBFTC DLETE. DECK
    SUBROUTINE DLETE ( IRHS, NROW, NRP1, NCOL, NM, * )
    COMMON /JRHS/ JRHS(100)
    COMMON /BIN1/ NW, NX, XL(2), Z(20), U(20,20)
    COMMON /DLT/ NWW, NXX
    COMMON /PRTCTL/ WRITE
    LOGICAL WRITE
    KRHS = 2 * IRHS
    IF ( KRHS .GT. 100 ) GO TO 900
    READ (5,500) (JRHS(I),I=1,KRHS)
    IF ( WRITE ) WRITE (6,601) IRHS, (JRHS(I),I=1,KRHS)
    DO 10 I = 1,KRHS,2
    K = JRHS(I)
    L = JRHS(I+1)
10   U(K,L) = 0.
    NWW = NW
    I = 0
    DO 30 K = 1,NW
    USUM = 0.
    DO 20 L = 1,NX
20   USUM = USUM + U(K,L)
    IF ( USUM .EQ. 0. ) GO TO 28
    I = I + 1
    DO 25 J = 1,NX
25   U(I,J) = U(K,J)
    XL(I) = XL(K)
    GO TO 30
28   NWW = NWW- 1
30   CONTINUE
    NXX = NX
    J = 0
    DO 50 L = 1,NX
    USUM = 0.
    DO 40 K = 1,NWW
40   USUM = USUM + U(K,L)
    IF ( USUM .EQ. 0. ) GO TO 48
    J = J + 1
    DO 45 I = 1,NWW
45   U(I,J) = U(I,L)
    Z(J) = Z(L)
    GO TO 50
48   NXX = NXX - 1
50   CONTINUE
    NROW = NXX * NWW
    NRP1 = NROW + 1
    NCOL = NM + (2*NROW)
    IF ( .NOT. WRITE ) RETURN
    WRITE (6,602) NWW, NXX
    DO 60 I = 1,NWW
60   WRITE (6,603) I, (U(I,J),J=1,NXX)
    RETURN
900  WRITE (6,600) IRHS
    RETURN 1
500  FORMAT ( 27( 2I1,1X) )
600  FORMAT ( 45HNUMBER OF U MATRIX DELETIONS GREATER THAN 50 /
     X           7H0IRHS = I4 )
601  FORMAT ( 1HA, I3, 41H ELEMENTS OF MATRIX -U- HAVE BEEN DELETED /
     X           33(2X,2I1) )
602  FORMAT ( 20HAU MATRIX (ADJUSTED), I10, 5H ROWS, I6, 8H COLUMNS )
603  FORMAT ( 4H0ROW, I4, 1X, 6E20.7 / (9X, 6E20.7) )
    END

```

```

$1BFTC LPS. DECK
SUBROUTINE LPS ( * )
COMMON IE(20), E(51,51), X(51), P(51), Y(51), JH(51),
X KB(120), KOUT(7), ERR(8) LPS.0001
LPS.0002
COMMON /BIN1/ NW, NX, XL(20), Z(20), U(20,20) LPS.0003
LPS.0004
COMMON /BLPS/ N, NM, BF(20,50), BM(20,50), K LPS.0005
LPS.0006
COMMON /DLT/ NWW, NXX LPS.0007
COMMON /PRTCTL/ WRTTF LPS.0008
DIMENSION A(51,120), B(51), INFIX(8), TOL(4), BA(400) LPS.0009
DIMENSIION ABR(50), BS(51) LPS.0010
LOGICAL WRITE LPS.0011
DATA NMAX/50/, NMMAX/20/, NCOLMX/120/, NROWMX/50/ LPS.0012
NAME LIST /LP/ XM11, G, NM, N, IRHS,PERT LPS.0013
PERT = 0. LPS.0014
TRHS = 0 LPS.0015
READ (5,LP) LPS.0016
IF ( WRITE ) WRITE (6,600) XM11, G, NM, N LPS.0017
IF ( N .GT. NMAX ) GO TO 900 LPS.0018
IF ( NM .GT. NMMAX ) GO TO 904 LPS.0019
NROW = NW * NX LPS.0020
IF ( NROW .GT. NROWMX ) GO TO 902 LPS.0021
NCOL = NM + (2*NROW) LPS.0022
IF ( NCOL .GT. NCOLMX ) GO TO 901 LPS.0023
NRP1 = NROW + 1 LPS.0024
NWW = NW LPS.0025
NXX = NX LPS.0026
IF ( IRHS .GT. 0 ) LPS.0027
X CALL DDELETE ( IRHS, NROW, NRP1, NCOL, NM, $903 ) LPS.0028
20 DO 30 I = 1,NRP1 LPS.0029
DO 30 J = 1,NCOL LPS.0030
30 A(I,J) = 0. LPS.0031
DO 35 I = 1,NMMAX LPS.0032
DO 35 J = 1,NMAX LPS.0033
35 BF(I,J) = 0. LPS.0034
INFIX(1) = 4 LPS.0035
INFIX(2) = NCOL LPS.0036
INFIX(3) = 51 LPS.0037
INFIX(4) = NRP1 LPS.0038
INFIX(5) = 2 LPS.0039
INFIX(6) = 1 LPS.0040
INFIX(7) = 500 LPS.0041
INFIX(8) = 20 LPS.0042
TOL(1) = 1.E-7 LPS.0043
TOL(2) = 1.E-7 LPS.0044
TOL(3) = 1.E-6 LPS.0045
TOL(4) = 1.E-10 LPS.0046
PRM = 0. LPS.0047
R(1) = 0. LPS.0048
DO 50 I = 1,NROW LPS.0049
IN = (I-1) / NXX LPS.0050
K = IN + 1 LPS.0051
L = I - (IN*NXX) LPS.0052
R(I+1) = U(K,L) LPS.0053
IF ( PERT .GT. 0. ) B(I+1) = B(I+1)*(1.+2.*PERT*(FLRAN(X)-.5)) LPS.0054
50 BS(I+1) = B(I+1) LPS.0055
LN = 1 LPS.0056
SQRTG = SQRT( G ) LPS.0057
GMG = SQRTG - (1. / SQRTG) LPS.0058
XN = 1. / FLOAT(N) LPS.0059
RM(1,1) = XM11 LPS.0060
NROWS = NROW LPS.0061

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55 IF ( WRITE ) WRITE (6,612) LN, N          LPS.0062
  NROW = NROWS                                LPS.0063
  NRP1 = NROW + 1                             LPS.0064
  DO 60 J = 1,NM                            LPS.0065
  RM(J,LN) = RM(1,LN)* G** (J-1)            LPS.0066
  DBM = GMG * RM(J,LN)                      LPS.0067
  DO 60 I = 1,NROW                          LPS.0068
  IN = (I-1) / NXX                         LPS.0069
  K = IN +1                                 LPS.0070
  L = I- (IN*NXX)                           LPS.0071
  XLKM = XL(K) * BM(J,LN)                  LPS.0072
  XNUM = XLKM**2 * EXP( -XLKM * Z(L) )    LPS.0073
  DENOM= 1. - EXP( -XLKM )                 LPS.0074
  60 A(I+1,J) = (XNUM / DENOM) * DBM       LPS.0075
  IT = 1                                    LPS.0076
  DO 64 I = 2,NRP1                         LPS.0077
  R(I) = RS(I)                            LPS.0078
  IF ( R(I) .EQ. 0. ) GO TO 64             LPS.0079
  II = II + 1                            LPS.0080
  B(II) = B(I)                           LPS.0081
  DO 62 J = 1,NM                         LPS.0082
  62 A(II,J) = A(I,J)                   LPS.0083
  64 CONTINUE                                LPS.0084
  NRP1 = II                                 LPS.0085
  NROW = NRP1 - 1                         LPS.0086
  INFIX(4) = NRP1                        LPS.0087
  J = NM                                    LPS.0088
  DO 68 I = 2,NRP1                         LPS.0089
  J = J + 1                               LPS.0090
  A(I,J) = 1.0                            LPS.0091
  A(I,J) = 1.0                            LPS.0092
  J = J + 1                               LPS.0093
  A(I,J) = 1.0                            LPS.0094
  68 A(I,J) = -1.0                         LPS.0095
  CALL DETA ( A, BA, NM, NROW )           LPS.0096
  IF ( WRITE ) WRITE (6,601) (M,M=1,30)     LPS.0097
  DO 80 I = 2,NRP1                         LPS.0098
  DO 70 J = 1,NM                           LPS.0099
  TF(J) = -99                             LPS.0100
  70 IF ( A(I,J) .NE. 0. ) IF(J) = ALOG10( A(I,J) )
  TM1 = T - 1                            LPS.0101
  80 IF ( WRITE ) WRITE (6,602) IM1, (IF(J),J=1,NM) LPS.0102
  CALL SIMPLX ( INFIX, A, B, TOL, PRM, KOUT, ERR, JH, X, P, Y, KB,E )LPS.0103
  IF ( WRITE ) WRITE (6,603)                LPS.0104
  DO 90 J = 1,NRP1                         LPS.0105
  MX = JH(J)                            LPS.0106
  90 IF ( (MX .GT. 0) .AND. (MX .LE. NM) ) BF(MX,LN) = X(J) LPS.0107
  ABR(LN) = 0.                            LPS.0108
  DO 110 I = 2,NRP1                         LPS.0109
  BC = 0.                                LPS.0110
  DO 100 J = 1,NM                           LPS.0111
  100 BC = BC + BF(J,LN) * A(I,J)          LPS.0112
  BD = R(I) - BC                         LPS.0113
  AR = ABS( BD ) / B(I)                  LPS.0114
  IF ( WRITE ) WRITE (6,604) B(I), BC, BD, AR LPS.0115
  110 ABR(LN) = ABR(LN) + AR             LPS.0116
  ABR(LN) = ABR(LN) / FLOAT( NROW )      LPS.0117
  IF ( .NOT. WRITE ) GO TO 115            LPS.0118
  WRITE (6,605) ABR(LN)                  LPS.0119
  WRITE (6,606) LN, (BF(M,LN),M=1,NM)    LPS.0120
  WRITE (6,610)                          LPS.0121
                                         LPS.0122

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115 LN = LN + 1          LPS.0123
    IF ( LN .GT. N ) GO TO 120   LPS.0124
    RM(1,LN) = RM(1,LN-1) * G**XN   LPS.0125
    GO TO 55   LPS.0126
120 IF ( WRITE ) WRITE (6,610)   LPS.0127
    WRITE (6,615)   LPS.0128
    ARBAVG = 0.   LPS.0129
    DO 130 I = 1,N   LPS.0130
    ARBAVG = ARBAVG + ABR(I)   LPS.0131
130 WRITE (6,614) I, ABR(I), (BF(M,I),M=1,NM)   LPS.0132
    ARBAVG = ARBAVG / FLOAT( N )   LPS.0133
    WRITE (6,613) ARBAVG   LPS.0134
    CALL ORDER ( RM, BF, NM, N, K )   LPS.0135
    RETURN   LPS.0136
900 WRITE (6,607) N   LPS.0137
    RETURN 1   LPS.0138
901 WRITE (6,608) NCOL   LPS.0139
    RETURN 1   LPS.0140
902 WRITE (6,609) NROW   LPS.0141
903 RETURN 1   LPS.0142
904 WRITE (6,611) NM   LPS.0143
    RETURN 1   LPS.0144
600 FORMAT ( 33HAFIRST MOLECULAR WEIGHT      = E16.7 /   LPS.0145
    X      33H MOLECULAR WEIGHT MULTIPLIER     = E16.7 /   LPS.0146
    X      33H NUMBER OF MOLECULAR WT. VALUES = 18      /   LPS.0147
    X      33H NUMBER OF LP SETS FOR SOLUTION = 18      )   LPS.0148
601 FORMAT ( 1HA, 57X, 14HA MATRIX (LOG) / 1H0, 60X, 7HCOLUMNS /   LPS.0149
    X      5H ROWS, 30I4 / 1H )   LPS.0150
602 FORMAT ( 1X, I3, 1X, 30I4 / ( 5X, 30I4 ) )   LPS.0151
603 FORMAT ( 1H1, 7X, 9HINPUT RHS, 7X, 12HCOMPUTED RHS, 6X,   LPS.0152
    X      14HRHS DIFFERENCE, 4X, 16HARS REL DIFF RHS / 1H )LPS.0153
604 FORMAT ( 1X, 4E18.7 )   LPS.0154
605 FORMAT ( 34HOAVERAGE RELATIVE DIFFERENCE RHS = E16.7 )   LPS.0155
606 FORMAT ( 9HOSOLUTION, I4, 7X, 7E16.7 / (20X, 7E16.7) )   LPS.0156
607 FORMAT ( 4HON = I4, 42H IS GREATER THAN DIMENSION FOR NO. OF SETS)LPS.0157
608 FORMAT ( 56HONNUMBER OF COLUMNS FOR -A- MATRIX GREATER THAN DIMENSILPS.0158
    XON / 7HONROW = I4 )   LPS.0159
609 FORMAT ( 53HONNUMBER OF ROWS FOR -A- MATRIX GREATER THAN DIMENSION LPS.0160
    X / 7HOROW = I4 )   LPS.0161
610 FORMAT ( 1H1 )   LPS.0162
611 FORMAT ( 5HONM = I4, 59H IS GREATER THAN DIMENSION FOR NUMBER OF SLPS.0163
    XOLUTIONS PER SET )   LPS.0164
612 FORMAT ( 1H0, 57X, 3HSET I3, 3H OF I3 )   LPS.0165
613 FORMAT ( 1H0 / 20X, 38HTHE AVERAGE REL. DIFF. FOR ALL SETS IS   LPS.0166
    X      E16.7 )   LPS.0167
614 FORMAT ( 1H0, I4, E22.7, 9X, 6E16.7 / (36X, 6E16.7) )   LPS.0168
615 FORMAT (6H0 SFT,6X,15HAVG. RFL. ERROR,12X,11HSOLUTIONS ,82(1H*) LPS.0169
    X      / 1H )   LPS.0170
    END   LPS.0171

```

```

*TRFTC IN1. DECK
SUBROUTINE IN1( * )
COMMON /BLOCKR/ X(20)
COMMON /BLOCKC/ C0(160)
COMMON /BLOCKW/ W2(20)
COMMON /BIN1/ NW, NX, XL(20), Z(20), U(20,20)
COMMON /BIN2/ USEIN2
COMMON /RINP1/ DH, H, NC, F(162), H0(162), SKIP2
COMMON /PRTCTL/ WRITE
C
      DATA  NXMAX/20/, NHMAX/160/, NWMAX/20/
C
      LOGICAL WRITE, SKIP1, SKIP2
      LOGICAL USEIN2
C
      NAME LIST /INP1/ NW, NX, H1, DH, NH, H, CZ, X1, DX,
      X           IST, LST, LAST, WRITE, SKIP1, SKIP2, USEIN2
C
      WRITE = .FALSE.
      SKIP1 = .FALSE.
      SKIP2 = .FALSE.
      USEIN2 = .FALSE.
      LAST = 1
      READ( 5,INP1)
      IF( LAST .EQ. 0 ) RETURN 1
      IF( SKIP1 ) GO TO 75
      IF( NX .GT. NXMAX ) GO TO 900
      IF( NH .GT. NHMAX ) GO TO 901
      IF( NW .GT. NWMAX ) GO TO 902
      IF( USEIN2 ) CALL IN2( $85 )
      NC = LST - IST + 1
      IF( NC .GT. NHMAX ) GO TO 903
      IF( X1 .LE. 0. ) GO TO 5
      X(1) = X1
      DO 10 L = 2,NX
      10 X(L) = X1 + FLOAT(L-1) * DX
      5 H0(1) = H1
      H0(1) = H1
      DO 20 N = 2,NH
      20 H0(N) = H1 + FLOAT(N-1) * DH
      DO 30 I = 1,NC
      IC = I + IST - 1
      F(I) = C0(IC) / CZ
      30 H0(I) = H0(IC) / H
      B = X(NX)
      RMM = B - X1
      DO 40 K = 1,NW
      40 XL(K) = RMM * H * W2(K)
      DO 50 L = 1,NX
      50 Z(L) = (B - X(L)) / RMM
      DO 70 K = 1,NW
      DO 70 L = 1,NX
      U(K,L) = 0.
      DO 70 N = 1,NC
      XLM = XL(K) * H0(N)
      XNUM = XLM**2 * EXP( -XLM*Z(L) )
      DENOM = 1. - EXP( -XLM )
      70 U(K,L) = U(K,L) + (XNUM / DENOM) * F(N)
      75 IF( .NOT. WRITE ) GO TO 85
      WRITE( 6,601) NW, (W2(K),K=1,NW)
      WRITE( 6,602) NX, (Z(L),L=1,NX)

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PART III

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      WRITE (6,603) NW, NX          IN1.0062
      DO 80 K = 1,NW              IN1.0063
 80   WRITE (6,604) K, (U(K,L),L=1,NX)    IN1.0064
      85 RETURN                   IN1.0065
 900  WRITE (6,605) NX           IN1.0066
      STOP                      IN1.0067
 901  WRITE (6,606) NH           IN1.0068
      STOP                      IN1.0069
 902  WRITE (6,607) NW           IN1.0070
      STOP                      IN1.0071
 903  WRITE (6,608) NC           IN1.0072
      STOP                      IN1.0073
 601 FORMAT ( 1HA, I4, 40H VALUES OF ANGULAR VELOCITY SQUARED - W2 /    IN1.0074
      X             1H / ( 9X, 6E20.7 ) )          IN1.0075
 602 FORMAT ( 1H0, I4, 71H VALUES OF THE FUNCTION OF DISTANCE SQUARED FIN1.0076
      XROM CENTER OF ROTATION - Z / 1H / ( 9X, 6E20.7 ) )          IN1.0077
 603 FORMAT ( 9HOU MATRIX, I10, 5H ROWS, I6, 8H COLUMNS )          IN1.0078
 604 FORMAT ( 4HORROW, I4, 1X, 6E20.7, / ( 9X, 6E20.7 ) )          IN1.0079
 605 FORMAT ( 5HONX = I4, 33H IS GREATER THAN DIMENSION FOR X. )       IN1.0080
 606 FORMAT ( 5HONH = I4, 33H IS GRFATER THAN DIMFNSION FOR H. )       IN1.0081
 607 FORMAT ( 5HONW = I4, 37H IS GREATER THAN DIMENSION FOR OMEGA. )    IN1.0082
 608 FORMAT ( 5HONC = I4, 41H IS GREATER THAN DIMENSION FOR SELECTED H)IN1.0083
      FND                      IN1.0084
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$IBFTC IN2. DECK           IN2.0001
      SUBROUTINE IN2 ( * )   IN2.0002
      SCRATCH STORAGE       IN2.0003
      COMMON DCDX(20,20)     IN2.0004
      DIMENSION DNDR(20,20)  IN2.0005
      LOGICAL WRITE          IN2.0006
      COMMON /BIN1/ NW, NR, XL(20), Z(20), U(20,20) IN2.0007
      COMMON /BLOCKW/ W2(20)  IN2.0008
      COMMON /BLOCKR/ X(20)   IN2.0009
      COMMON /PRTCTL/ WRITE   IN2.0010
      DATA NRMAX/20/, NWMAX/20/ IN2.0011
      NAME LIST /INP2/ NW, NR, H, C0, R1, DR, DCDN, DNDR, W2 IN2.0012
      READ (5,INP2)             IN2.0013
      IF ( NR .GT. NRMAX ) GO TO 900 IN2.0014
      IF ( NW .GT. NWMAX ) GO TO 901 IN2.0015
      DO 10 L = 1,NR             IN2.0016
      IF ( R1 .LE. 0. ) GO TO 5   IN2.0017
      X(L) = ( R1 + FLOAT(L-1) * DR )**2 IN2.0018
      5 DO 10 K = 1,NW            IN2.0019
      10 DCDX(K,L) = 1.0 / SQRT(X(L)) * DCDN * DNDR(K,L) IN2.0020
      XM = X(1)                  IN2.0021
      R = X(NR)                  IN2.0022
      DO 20 K = 1, NW            IN2.0023
      20 XL(K) = (B-XM) * H * W2(K) IN2.0024
      DO 30 L = 1, NR            IN2.0025
      30 Z(L) = (B-X(L)) / (B-XM) IN2.0026
      DO 40 L = 1,NR             IN2.0027
      DO 40 K = 1,NW             IN2.0028
      40 U(K,L) = ((B-XM) / C0) * DCDX(K,L) IN2.0029
      IF ( .NOT. WRITE ) GO TO 60 IN2.0030
      WRITE (6,601) NW, (W2(K),K=1,NW) IN2.0031
      WRITE (6,602) NR, (Z(L),L=1,NR) IN2.0032
      WRITE (6,603) NW, NR           IN2.0033
      DO 50 K = 1,NW             IN2.0034
      50 WRITE (6,604) K, (U(K,L),L=1,NR) IN2.0035
      60 RETURN 1                IN2.0036
      900 WRITE (6,605) NR, NRMAX  IN2.0037
      STOP                      IN2.0038
      901 WRITE (6,606) NW, NWMAX  IN2.0039
      STOP                      IN2.0040
      601 FORMAT ( 1HA, I4, 40H VALUES OF ANGULAR VELOCITY SQUARED - W2 /
      X      1H / ( 9X, 6E20.7 ) ) IN2.0041
      602 FORMAT ( 1H0, I4, 71H VALUES OF THE FUNCTION OF DISTANCE SQUARED FIN2.0042
      XROM CENTER OF ROTATION - Z / 1H / ( 9X, 6E20.7 ) ) IN2.0043

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```
603 FORMAT ( 9HOU MATRIX, I10, 5H ROWS, I6, 8H COLUMNS )           IN2•0062
604 FORMAT ( 4H0ROW, I4, 1X, 6E20.7 / ( 9X, 6E20.7 ) )          IN2•0063
605 FORMAT ( 5H0NR = I4, 33H IS GREATER THAN DIMENSION FOR X(,I2,2H).)IN2•0064
606 FORMAT ( 5H0NW = I4, 33H IS GREATER THAN DIMENSION FOR W(,I2,2H).)IN2•0065
C
      END                                         IN2•0066
                                                IN2•0067
```

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$IBFTC DET. DECK          L. B. FALL      DET.0001
FUNCTION DET(A,N)          DET.0002
C
C           DETERMINANT EVALUATING FUNCTION
C
C           FUNCTION DFT(A,N) COMPUTES THE DETERMINANT
C           OF THE N-TH ORDER MATRIX A, WHICH MUST BE
C           DIMENSIONED A(N,N).  THE ORIGINAL MATRIX A
C           IS NOT ALTERED.
C
C           612 CELLS OF BLANK COMMON ARE USED
C
C           TO CHANGE DIMENSIONS, CHANGE DIMENSIONS OF ARRAYS B AND PIV,
C           AND ALSO CHANGE VALUE OF NMAX IN THE DATA STATEMENT.
C
C           DIMENSION A(N,N)
COMMON   D, I, II, J, K, KCT, KFROM, KTO, NN, NPR, RLE, TPE
COMMON   B(24,24), PIV(24)
DATA    NMAX/ 24/
C
C           TEST ARGUMENT N TO PREVENT OVERFLOWING BLANK COMMON
C
C           NN=N
IF ( NN .GT. NMAX .OR. NN .LE. 0 )      GO TO 100
C
C           MOVE INPUT MATRIX A TO SCRATCH MATRIX B
C
DO 10 I=1,NN
DO 10 J=1,NN
10  B(I,J)=A(I,J)
C
C           INITIALIZE DETERMINANT VALUE AND ROW INTERCHANGE COUNT
C
D=1.0
KCT=0
C
C           PERFORM ELIMINATION ON N COLUMNS
C
DO 90 I=1,NN
C
C           SEARCH I-TH SUB-COLUMN FOR I-TH PIVOT ELEMENT
C
TPF=0.
DO 30 II=I,NN
IF (ARS(B(II,I))-TPF) 30,20,20
20  NPR=II
TPF=ARS(B(II,I))
30  CONTINUE
C
C           IF PIVOT ELEMENT IS ZERO, THEN DET(A,N)=0.0
C
IF (B(NPR,I)) 35,32,35
32  D=0.
GO TO 95
C
C           DIVIDE PIVOT ROW BY PIVOT ELEMENT
C
35  DO 40 J=1,NN
40  PIV(J)=B(NPR,J)/B(NPR,I)
C
C           UPDATE THE PRODUCT OF PIVOT ELEMENTS AND SUM OF ROW INTERCHANGES
DET.0003
DET.0004
DET.0005
DET.0006
DET.0007
DET.0008
DET.0009
DET.0010
DET.0011
DET.0012
DET.0013
DET.0014
DET.0015
DET.0016
DET.0017
DFT.0018
DET.0019
DET.0020
DET.0021
DET.0022
DET.0023
DET.0024
DET.0025
DET.0026
DET.0027
DET.0028
DET.0029
DET.0030
DET.0031
DET.0032
DET.0033
DET.0034
DET.0035
DFT.0036
DET.0037
DET.0038
DET.0039
DET.0040
DET.0041
DET.0042
DET.0043
DET.0044
DET.0045
DET.0046
DET.0047
DET.0048
DET.0049
DET.0050
DET.0051
DET.0052
DET.0053
DET.0054
DET.0055
DET.0056
DET.0057
DET.0058
DFT.0059
DET.0060
DET.0061

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```
C      D=D*B(NPR,I)          DET.0062
C      KCT=KCT+(NPR-I)        DET.0063
C
C      ELIMINATE REMAINING ELEMENTS IN I-TH SUB-COLUMN    DET.0064
C
C      KTO=NN              DET.0065
C      KFROM=NN             DET.0066
C      DO 90 K=I,NN          DET.0067
C      IF (KFROM=NPR) 70,80,70   DET.0068
70     RLE=-B(KFROM,I)       DET.0069
      DO 75 J=I,NN           DET.0070
75     B(KTO,J)=B(KFROM,J)+RLE*PIV(J)      DET.0071
      KTO=KTO-1            DET.0072
80     KFROM=KFROM-1        DET.0073
90     CONTINUE             DET.0074
C
C      IF TOTAL NO. OF ROW INTERCHANGES WAS ODD, THEN    DET.0075
C      NEGATE THE PRODUCT OF THE PIVOT ELEMENTS         DET.0076
C
C      95 IF ( KCT .NE. 2*(KCT/2) )      D=-D      DET.0077
      DET=D               DET.0078
      RETURN              DET.0079
C
C      GIVE ERROR MESSAGE FOR INCORRECT VALUE OF N        DET.0080
C      AND RETURN TO SYSTEM VIA FXEM                      DET.0081
C
100    WRITE (6,1000) NN          DET.0082
      CALL FXEM            DET.0083
      RETURN              DET.0084
C
C      1000 FORMAT (3H0N=,I12,30H IS INCORRECT FOR FUNCTION DET)  DET.0085
      END                  DET.0086
                                         DET.0087
                                         DET.0088
                                         DET.0089
                                         DET.0090
                                         DET.0091
                                         DET.0092
                                         DET.0093
                                         DET.0094
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$IBFTC MSUB      DECK                               MSUB.001
CMSUBJ      VERSION 1 OF   RS MSUB               MSUB.002
            SUBROUTINE SIMPLX (INFIX,A,B,TOL,PRM,KOUT,ERR,JH,X,P,Y,KB,E)  MSUB.003
C           DIMENSION INFIX(8),A(1),B(1),TOL(4),KOUT(7),ERR(8),JH(1),X(1),  MSUB.004
1 P(1),Y(1),KB(1),F(1),ZZ(3), IOFIX(16) , TFRR(8)  MSUB.005
C           EQUIVALENCE (INFLAG,IOFIX(1) ), (N , IOFIX(2) ) ,  MSUB.006
1 (ME,IOFIX(3) ), (M,IOFIX(4)), (MF,IOFIX(5)),  MSUB.007
2 (MC, IOFIX(6) ), ( NCUI, IOFIX(7) ) , ( NVER, IOFIX(8) ),  MSUB.008
3 ( K, IOFIX(9) ), ( IIER, IOFIX(10) ), ( INVc , IOFIX(11) ) ,  MSUB.009
4 ( NUMVR, IOFIX(12) ), ( NUMPv, IOFIX(13) ) ,  MSUB.010
5 (INFS, IOFIX(14) ) , ( JT, IOFIX(15) ) ,( LA , IOFIX(16) ),  MSUB.011
6 (ZZ(1),TPIV), (ZZ(2),TZERO),(ZZ(3),TCOST)  MSUB.012
C           MOVE INPUTS ... ZERO OUTPUTS  MSUB.013
C           DO 1340 I= 1, 8  MSUB.014
1340    TERR(I) = 0.0  MSUB.015
          IOFIX(I+8) = 0  MSUB.016
1340    IOFIX(I) = INFIX(I)  MSUB.017
          LA = 0  MSUB.018
1340    DO 1308 I = 1 , 3  MSUB.019
1308    ZZ(I) = TOL(I)  MSUB.020
          TCOST = - ABS (TCOST)  MSUB.021
          PMIX = PRM  MSUB.022
          M2 = M**2  MSUB.023
          INFS = 1  MSUB.024
C           CHECK FOR ILLEGAL INPUT  MSUB.025
          IF (N) 1304, 1304, 1371  MSUB.026
1371    IF (M - MF ) 1304, 1304, 1372  MSUB.027
1372    IF (MF - MC) 1304, 1304, 1373  MSUB.028
1373    IF ( MC ) 1304 , 1304, 1374  MSUB.029
1374    IF (ME - M ) 1304, 1375, 1375  MSUB.030
1375    IF( MOD (INFLAG, 4 ) - 1 ) 1400, 1320, 100  MSUB.031
C
C           NEW 1      STARTS PHASE CJE  MSUB.032
C*****SUBROUTINE NEW (M,N, JH, KB, A, B, MF, ME )  MSUB.033
C
C           INITIATE  MSUB.034
1400    DO 1401 I = 1, M  MSUB.035
1401    JH(I) = 0  MSUB.036
C           INSTALL SINGLETONS  MSUB.037
          KT = 0  MSUB.038
          DO 1402 J = 1, N  MSUB.039
          KB(J) = 0  MSUB.040
          MM = KT + MF  MSUB.041
          LL = KT + M  MSUB.042
C           TALLY ENTRIES IN CONSTRAINTS  MSUB.043
          KQ = 0  MSUB.044
          DO 1403 L = MM , LL  MSUB.045
          IF (A(L)) 1404, 1403, 1404  MSUB.046
1404    KQ = KQ+1  MSUB.047
          LQ = L  MSUB.048
1403    CONTINUE  MSUB.049
C           CHECK WHETHER J IS CANDIDATE  MSUB.050
          IF (KQ - 1) 1402, 1405, 1402  MSUB.051
1405    IA = LQ- KT  MSUB.052
          IF ( JH(IA) ) 1402, 1406, 1402  MSUB.053
1406    IF (A(LQ)*B(IA)) 1402, 1407, 1407  MSUB.054
C           J IS CANDIDATE. INSTALL  MSUB.055
          MSUB.056
          MSUB.057
          MSUB.058
          MSUB.059
          MSUB.060
          MSUB.061

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1407 JH(IA) = J          MSUB.062
    KB(J) = IA          MSUB.063
1402 KT = KT + ME       MSUB.064
C
C **END OF NEW
C
C
1320 CONTINUE
C
C VER 1      FORMS INVERSE FROM KB
C*****SUBROUTINE VER ( A, B, JH, X, E, KB, Y, IOFIX, TPIV, M2 )
C
C           INITIATE
1100 ASSIGN 1102 TO KPIV      MSUB.075
    ASSIGN 1114 TO KJMY      MSUB.076
    IF (LA) 1121, 1121, 1122  MSUB.077
1121 INV C = 0               MSUB.078
1122 NUMVR = NUMVR +1       MSUB.079
    DO 1101 I = 1, M2        MSUB.080
1101 E(I)=0.                 MSUB.081
    MM=1                     MSUB.082
    DO 1113 I = 1, M         MSUB.083
    E(MM) =1.0                MSUB.084
    X(I) = B(I)                MSUB.085
1113 MM = MM + M + 1        MSUB.086
    DO 1110 I = MF, M         MSUB.087
    IF (JH(I)) 1111, 1110, 1111  MSUB.088
1111 JH(I) = 12345
1110 CONTINUE
    INF S = 1
C           FORM INVERSE
    DO 1102 JT= 1, N         MSUB.092
    IF ( KB(JT)) 600 , 1102 , 600  MSUB.093
C 600 CALL JMY (JT, A, E, M, Y )  MSUB.094
C           CHOOSE PIVOT
1114 TY = 0.                 MSUB.095
    DO 1104 I = MF, M         MSUB.096
    IF (JH(I) - 12345 ) 1104, 1105, 1104  MSUB.097
1105 IF ( ABS ( Y(I) ) - TY ) 1104, 1104, 1106  MSUB.098
1106 IR = I                  MSUB.099
    TY = ABS ( Y(I) )        MSUB.100
1104 CONTINUE
C           TEST PIVOT
    IF (TY - TPIV ) 1107, 1108, 1108  MSUB.101
C           BAD PIVOT, ROW IR, COLUMN JT
1107 KB(JT)= 0                MSUB.102
    GO TO 1102
C           PIVOT
1108 JH(IR) = JT              MSUB.103
    KB(JT) = IR                MSUB.104
    GO TO 900
C 900 CALL PIV (IR, Y, M, E, Z, X)  MSUB.105
1102 CONTINUE
C           RESET ARTIFICIALS
    DO 1109 I = 1, M          MSUB.106
    IF ( JH(I) - 12345 ) 1109, 1112, 1109  MSUB.107
1112 JH(I) = 0                MSUB.108
1109 CONTINUE
C **END OF VFR
C
C

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100 ASSIGN    705 TO NDEL          MSUB.123
      ASSIGN   1000 TO KJMY         MSUB.124
      ASSIGN    221 TO KPIV         MSUB.125
C
C                               PERFORM ONE ITERATION
C
C XCK 1      X CHECKER          MSUB.126
C*****SUBROUTINE XCK ( M, MF, JH, X, TZERO, JIN )  MSUB.127
C
C           RESET X AND CHECK FOR INFEASIBILITIES
1200   JIN = 0                  MSUB.128
      NEG = 0                  MSUB.129
      DO 1201 I = MF, M        MSUB.130
      IF ( ABS ( X(I) ) - TZERO) 1202, 1203, 1203
1202   X(I) = 0.0               MSUB.131
      GO TO 1201               MSUB.132
1203   IF ( X(I) ) 1208, 1201, 1205  MSUB.133
1205   IF ( JH(I) ) 1201, 1206, 1201  MSUB.134
1208   NEG = 1                 MSUB.135
1206   JIN = 1                 MSUB.136
1201   CONTINUE                MSUB.137
C**END OF XCK                MSUB.138
C
C           CHECK CHANGE OF PHASE.. GO BACK TO INVERT IF GONE INFEAS.
      IF (INFS - JIN ) 1320, 500, 200  MSUB.139
C                           BECOME FEASIBLE
200  INFS = 0                 MSUB.140
201  PMIX = 0.0               MSUB.141
C
C GET 1      GET PRICES        MSUB.142
C*****SUBROUTINE GET ( M, MC, MF, JH, X, P, E, INFS, PMIX )
C
C 500 MM = MC                 MSUB.143
C                           PRIMAL PRICES
502  DO 503 J = 1, M        MSUB.144
      P(J) = E(MM)             MSUB.145
503  MM = MM + M            MSUB.146
      IF ( INFS ) 501, 599, 501  MSUB.147
C                           COMPOSITE PRICES
501  DO 504 J = 1, M        MSUB.148
      P(J) = P(J)* PMIX       MSUB.149
      DO 505 I = MF, M        MSUB.150
      MM = I                  MSUB.151
      IF ( X(I) ) 506, 507, 507  MSUB.152
506  DO 508 J = 1, M        MSUB.153
      P(J) = P(J) + E(MM)     MSUB.154
508  MM = MM + M            MSUB.155
      GO TO 505               MSUB.156
507  IF (JH(I)) 505, 509, 505  MSUB.157
509  DO 510 J = 1, M        MSUB.158
      P(J) = P(J) - E(MM)     MSUB.159
510  MM = MM + M            MSUB.160
505  CONTINUE                MSUB.161
C
      599 CONTINUE              MSUB.162
C**END OF GET                MSUB.163
C
C MIN          MIN D-J. SELECTS COLUMN TO ENTER BASIS
MSUB.164
MSUB.165
MSUB.166
MSUB.167
MSUB.168
MSUB.169
MSUB.170
MSUB.171
MSUB.172
MSUB.173
MSUB.174
MSUB.175
MSUB.176
MSUB.177
MSUB.178
MSUB.179
MSUB.180
MSUB.181
MSUB.182
MSUB.183

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*****SUBROUTINE MIN ( JT, N, M, A, P, KB, ME, ICOST )
C
  700 JT = 0
    BB = TCOST
C
  701 DO 702 JM = 1, N
          SKIP COLUMNS IN BASIS
  703 IF ( KB(JM) ) 702, 300, 702
C 300 CALL DEL ( JM, DT, M, A, P )
  705 IF ( DT - BB ) 708, 702, 702
    708 BB = DT
    JT = JM
  702    CONTINUE
C
C **END OF MIN
C
        IF ( JT) 203, 203, 600
C           ALL COSTS NON-NEGATIVE... K = 3 OR 4
  203 K = 3 + INFS
    GO TO 257
C
          NORMAL CYCLE
C
C JMY 1      J MULTIPLY. BASIS INVERSE * COLUMN JT
*****SUBROUTINE JMY (JT, A, E, M, Y, ME )
C
  600 DO 610 I= 1,M
  610 Y(I) =0.
    LP = JT*ME - ME
    LL = 0
    DO 605 I= 1,M
      LP = LP + 1
      IF (A(LP)) 601, 602, 601
  601 DO 606 J = 1,M
      LL = LL + 1
      606 Y(J) = Y(J) + A(LP) * E(LL)
      GO TO 605
  602 LL = LL + M
  605 CONTINUE
C
    699 GO TO KJMY , ( 1000 , 1114 , 1392 )
C **END OF JMY
C
C ROW 1      ROW SELECTION--COMPOSITE
*****SUBROUTINE ROW ( IR, M, MF, JH, X, Y, IPIV )
C
C AMONG EQS. WITH X=0, FIND MAX ABS(Y) AMONG ARTIFICIALS, OR, IF NONE,
C GET MAX POSITIVE Y(I) AMONG REALS.
  1000 IR = 0
    AA = 0.0
    IA = 0
    DO 1050 I = MF, M
      IF ( X(I) ) 1050, 1041, 1050
  1041 YI = ABS ( Y(I) )
      IF ( YI - TPIV ) 1050, 1050, 1042
  1042 IF ( JH(I) ) 1043, 1044, 1043
  1043 IF ( IA) 1050, 1048, 1050
  1048 IF ( Y(I) ) 1050, 1050, 1045
  1044 IF ( IA) 1045, 1046, 1045
  1045 IF ( YI - AA ) 1050, 1050, 1047
  1046 IA = 1

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1047 AA = YI                         MSUB.245
    IR = I                           MSUB.246
1050 CONTINUE                         MSUB.247
    IF (IR)1099,1001,1099             MSUB.248
1001 AA = 1.0E+20                     MSUB.249
C           FIND MIN. PIVOT AMONG POSITIVE EQUATIONS   MSUB.250
    DO 1010 IT = MF , M              MSUB.251
        IF ( Y(IT) - TPIV ) 1010, 1010, 1002
1002 IF ( X(IT) ) 1010, 1010, 1003   MSUB.252
1003 XY = X(IT) / Y(IT)            MSUB.253
        IF ( XY - AA ) 1004, 1005, 1010
1005 IF ( JH(IT) ) 1010, 1004, 1010   MSUB.254
1004 AA = XY                      MSUB.255
    IR = IT                          MSUB.256
1010 CONTINUE                         MSUB.257
    IF (NEG) 1016, 1099, 1016       MSUB.258
C   FIND PIVOT AMONG NEGATIVE EQUATIONS, IN WHICH X/Y IS LESS THAN THE
C   MINIMUM X/Y IN THE POSITIVE EQUATIONS, THAT HAS THE LARGEST ABSF(Y)   MSUB.259
1016 BB = - TPIV                     MSUB.260
    DO 1030 I = MF , M              MSUB.261
        IF (X(I)) 1012, 1030, 1030
1012 IF ( Y(I) - BB ) 1022, 1030, 1030   MSUB.262
1022 IF ( Y(I) * AA - X(I) ) 1024, 1024, 1030   MSUB.263
1024 BB = Y(I)
    IR = I
1030 CONTINUE                         MSUB.264
1099 CONTINUE                         MSUB.265
C**END OF ROW                         MSUB.266
C
C           TEST PIVOT
206   IF( IR ) 207, 207, 210          MSUB.267
C               NO PIVOT
207 K = 5                            MSUB.268
257 IF (PMIX) 201, 400, 201         MSUB.269
C           ITERATION LIMIT FOR CUT OFF   MSUB.270
210 IF (ITFR -NCUT ) 900, 160, 160   MSUB.271
C               PIVOT FOUND
C
C   PIV 1      PIVOT. PIVOTS ON GIVEN ROW   MSUB.272
C*****SUBROUTINE PIV ( IR, Y, M, E, X, NUMPV, TECOL )   MSUB.273
C               LEAVE TRANSFORMED COLUMN IN Y(I)   MSUB.274
C
900 NUMPV = NUMPV + 1                MSUB.275
    YI = -Y(IR)                      MSUB.276
    Y(IR) = -1.                       MSUB.277
    LL = 0                           MSUB.278
C           TRANSFORM INVERSOF
903 DO 904 L = IR, M2, M           MSUB.279
    IF ( F(L) ) 905, 914, 905
914 LL = LL + M                   MSUB.280
    GO TO 904
905 XY = E(L) / YI                MSUB.281
    E(L) =0.
    DO 906 I = 1, M
    LL= LL +1
906 E(LL) = E(LL) +XY* Y(I)
904 CONTINUE
C           TRANSFORM X
    XY = X(IR) / YI
    X(IR) = 0.
    DO 908 I = 1, M

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908 X(I) = X(I) +XY* Y(I) MSUB.306
C RESTORE Y(IR)
C Y(IR) = -YI MSUB.307
C
999 GO TO KPIV , ( 221, 1102 ) MSUB.308
C**END OF PIV MSUB.309
C
221 IA = JH(IR) MSUB.310
IF ( IA ) 213, 213, 214 MSUB.311
214 KB( IA ) = 0 MSUB.312
213 KB(JT) = IR MSUB.313
JH(IR) = JT MSUB.314
LA = 0 MSUB.315
ITER = ITER +1 MSUB.316
INVC = INVC +1 MSUB.317
C INVERSION FREQUENCY MSUB.318
IF (INVC - NVER ) 1200, 1320,1200 MSUB.319
C CUT OFF ... TOO MANY ITERATIONS MSUB.320
160 K = 6 MSUB.321
C
C
C ERR 1 ERROR CHECK. COMPARES AX WITH B, PA WITH ZERO MSUB.322
C*****SUBROUTINE ERR ( M, A, B, TERR, JH, X, P, Y, ME, LA ) MSUB.323
C
C STORE AX-B AT Y MSUB.324
400 ASSIGN 410 TO NDEL MSUB.325
DO 401 I = 1, M MSUB.326
401 Y(I) =-B(I) MSUB.327
DO 402 I = 1, M MSUB.328
JA = JH(I) MSUB.329
IF (JA) 403, 402, 403 MSUB.330
403 IA =ME* (JA-1) MSUB.331
DO 405 IT = 1, M MSUB.332
IA = IA + 1 MSUB.333
IF(A(IA) ) 415, 405, 415 MSUB.334
415 Y(IT) =Y(IT) +X(I) * A(IA) MSUB.335
405 CONTINUE MSUB.336
402 CONTINUE MSUB.337
C FIND SUM AND MAXIMUM OF ERRORS MSUB.338
DO 481 I = 1, M MSUB.339
YI = Y(I) MSUB.340
IF ( JH(I) ) 472, 471, 472 MSUB.341
471 YI = YI + X(I) MSUB.342
472 TERR(LA+1) = TERR(LA+1) + ABS (YI) MSUB.343
IF ( ABS (TERR(LA+2))- ABS ( YI ) ) 482, 481, 481 MSUB.344
482 TFRR(LA+2) = YI MSUB.345
481 CONTINUE MSUB.346
C STORE P TIMES BASIS AT DT MSUB.347
DO 411 I = 1, M MSUB.348
JM = JH(I) MSUB.349
IF ( JM ) 300 , 411 , 300 MSUB.350
C 300 CALL DEL ( JM, DT, M, A, P) MSUB.351
410 TERR(LA+3) = TERR(LA +3) + ABS (DT) MSUB.352
IF (ABS (TERR(LA+4)) - ABS (DT) ) 413, 411, 411 MSUB.353
413 TERR(LA+4) = DT MSUB.354
411 CONTINUE MSUB.355
C**END OF ERR MSUB.356
C
C
IF (LA) 193, 191, 193 MSUB.357
191 LA = 4 MSUB.358

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      IF (INFLAG - 4 ) 1320, 193, 193          MSUB.367
193 IF (K-5) 1392, 194, 1392          MSUB.368
194 ASSIGN 1392 TO KJMY          MSUB.369
      GO TO 600          MSUB.370
C 600 CALL JMY ( * * * * )
C  GO TO 1392          MSUB.371
1304 K = 7          MSUB.372
C           SET EXIT VALUES          MSUB.373
1392 DO 1309 I= 1, 8          MSUB.374
1309 ERR(I) = TERR(I)          MSUB.375
      DO 1329 I = 1, 7          MSUB.376
1329 KOUT(I) = IOFIX(I+8)          MSUB.377
      RETURN          MSUB.378
C
C     DEL           DELTA-JAY. PRICES OUT ONE MATRIX COLUMN          MSUB.379
C*****SUBROUTINE DEL ( JM, DT, M, A, P, ME )
C
C
300 DT = 0.          MSUB.380
      LL = (JM - 1) * ME          MSUB.381
301 DO 303 MM = 1, M          MSUB.382
      LL = LL + 1          MSUB.383
      IF ( A( LL ))304, 303, 304          MSUB.384
304 DT = DT + P( MM ) * A ( LL )          MSUB.385
303 CONTINUE          MSUB.386
C
399 GO TO NDEL , ( 410 , 705 )          MSUB.387
C**END OF DEL          MSUB.388
C
      END          MSUB.389
C
C

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## PART III

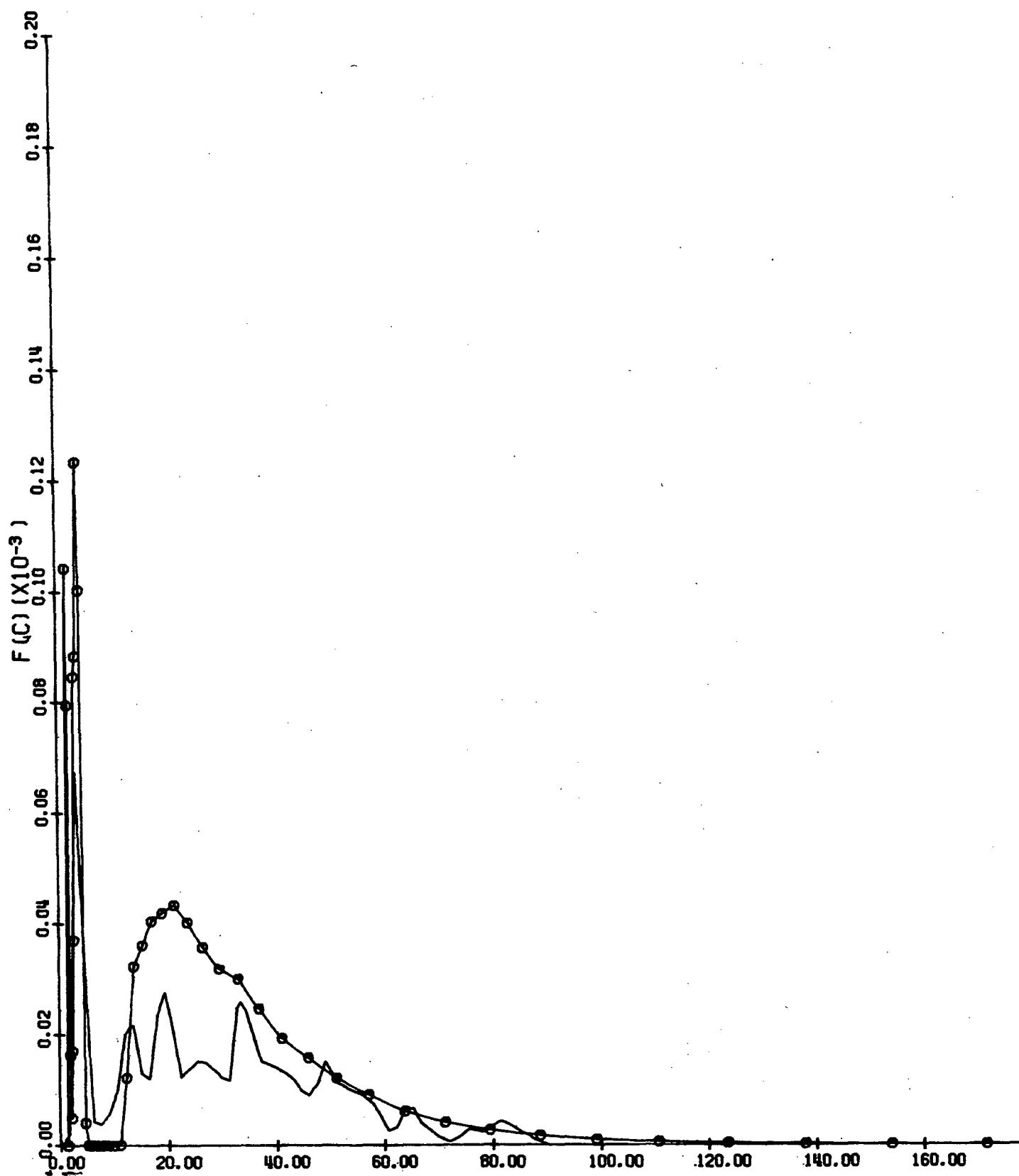
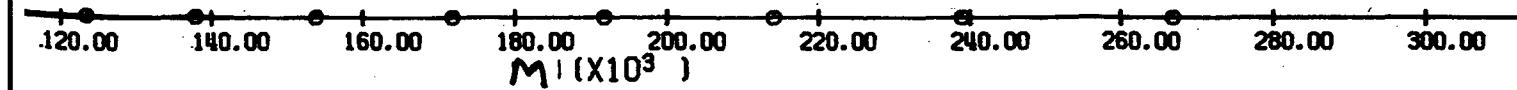


Figure 1. Resulting MWD Using Ten Sets of Molecular Weights a



Ten Sets of Molecular Weights and  $g = 3.0$ , (Compare with Figures 2~4)

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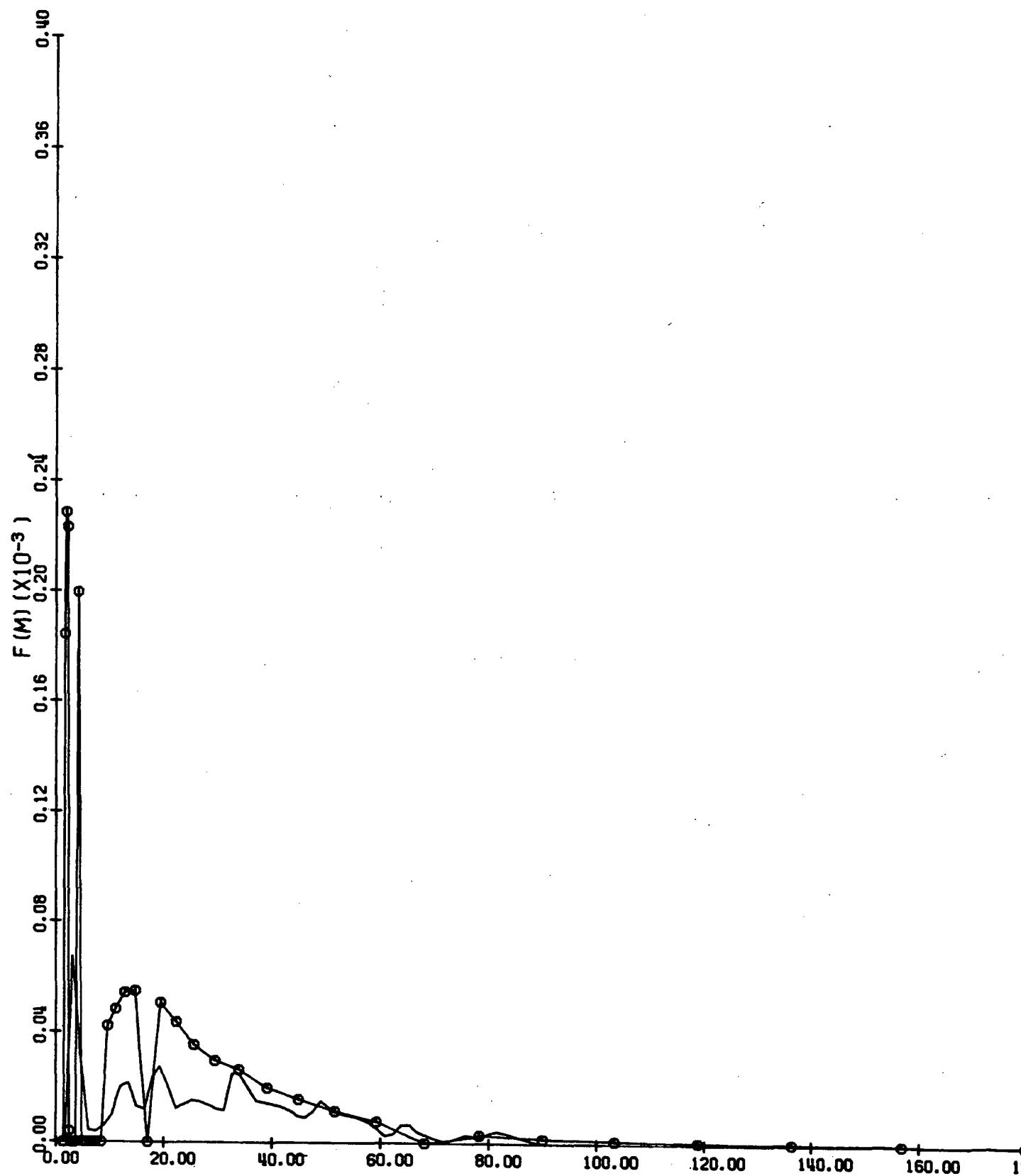
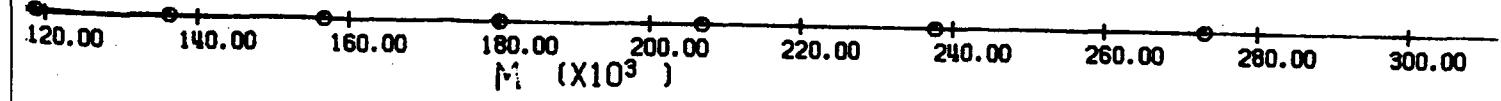


Figure 2. Resulting MWD Using Ten Sets of Molecular Weights and  $g = 1$



Sets of Molecular Weights and  $g = 4.0$ , (Compare with Figures 1, 3, and 4)

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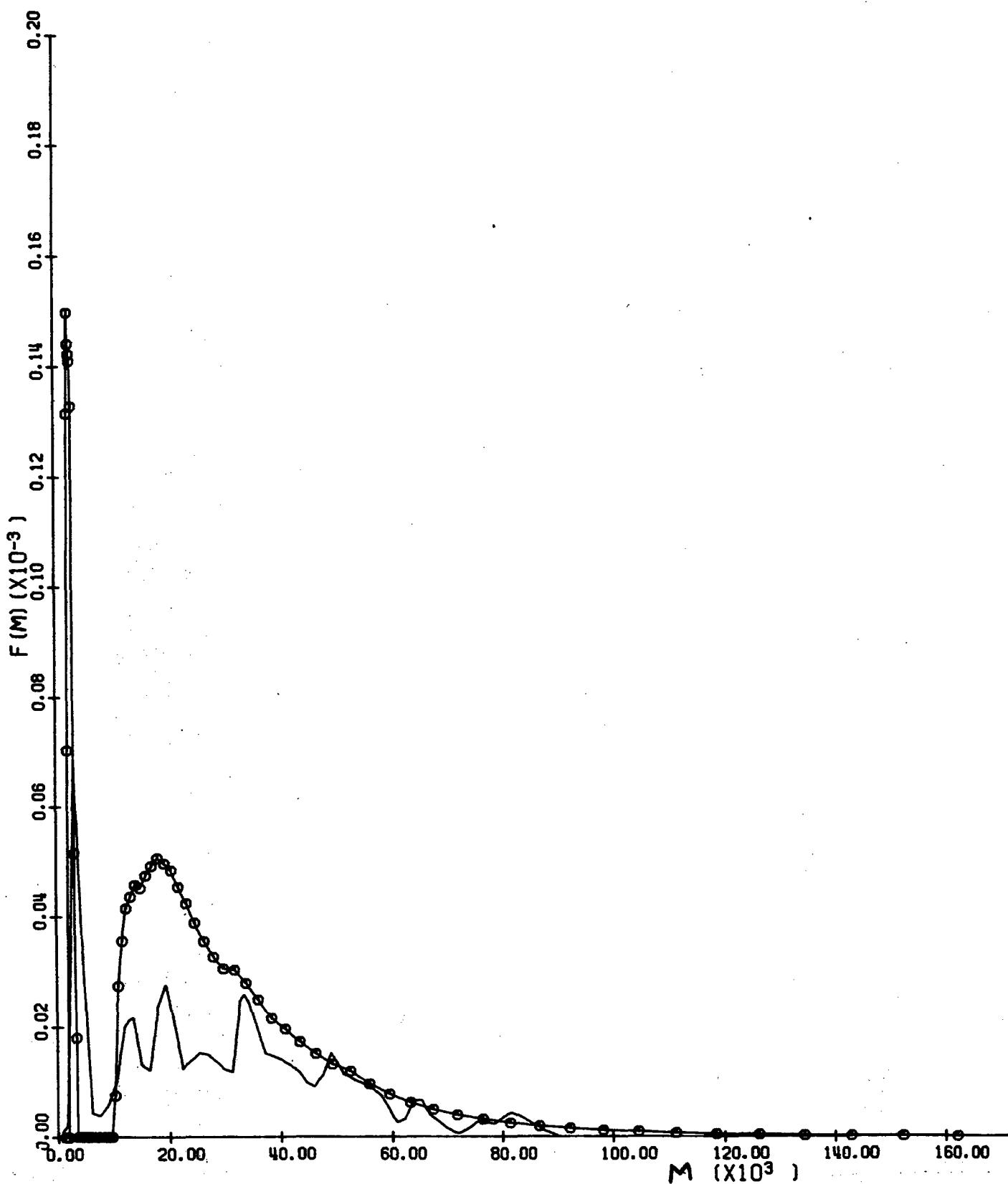
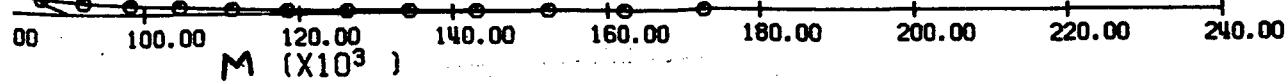


Figure 3. Resulting MWD Using Twenty Sets of Molecular Weights and  $g = 3.5$ , (Co



enty Sets of Molecular Weights and  $g = 3.5$ , (Compare with Figures 1, 2, and 4)

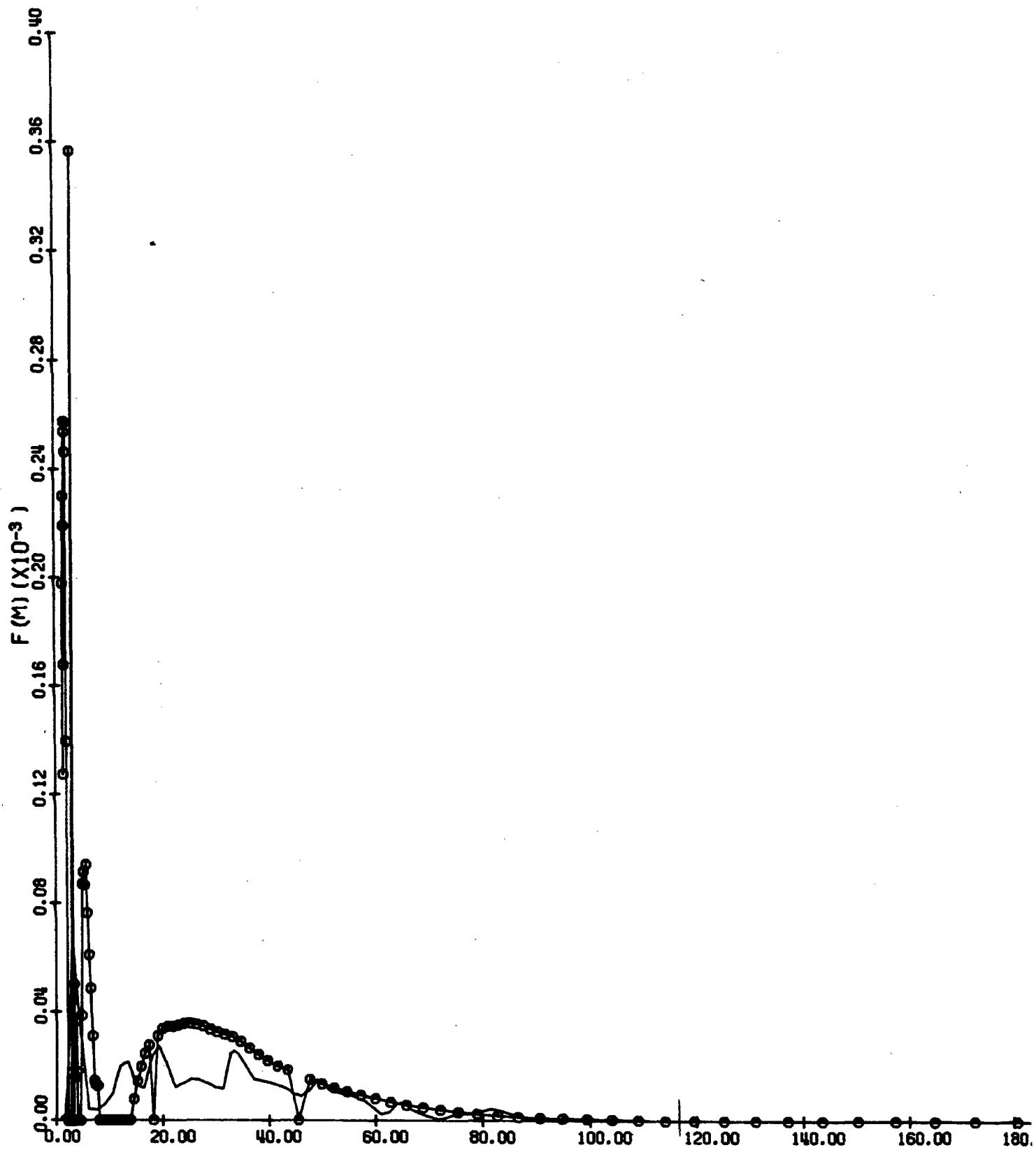
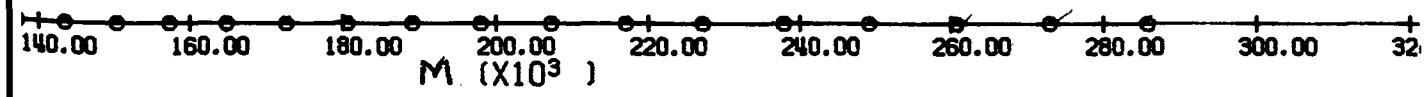


Figure 4. Resulting MWD Using Twenty Sets of Molecular W



enty Sets of Molecular Weights and  $g = 2.5$ , (Compare with Figures 1-3)

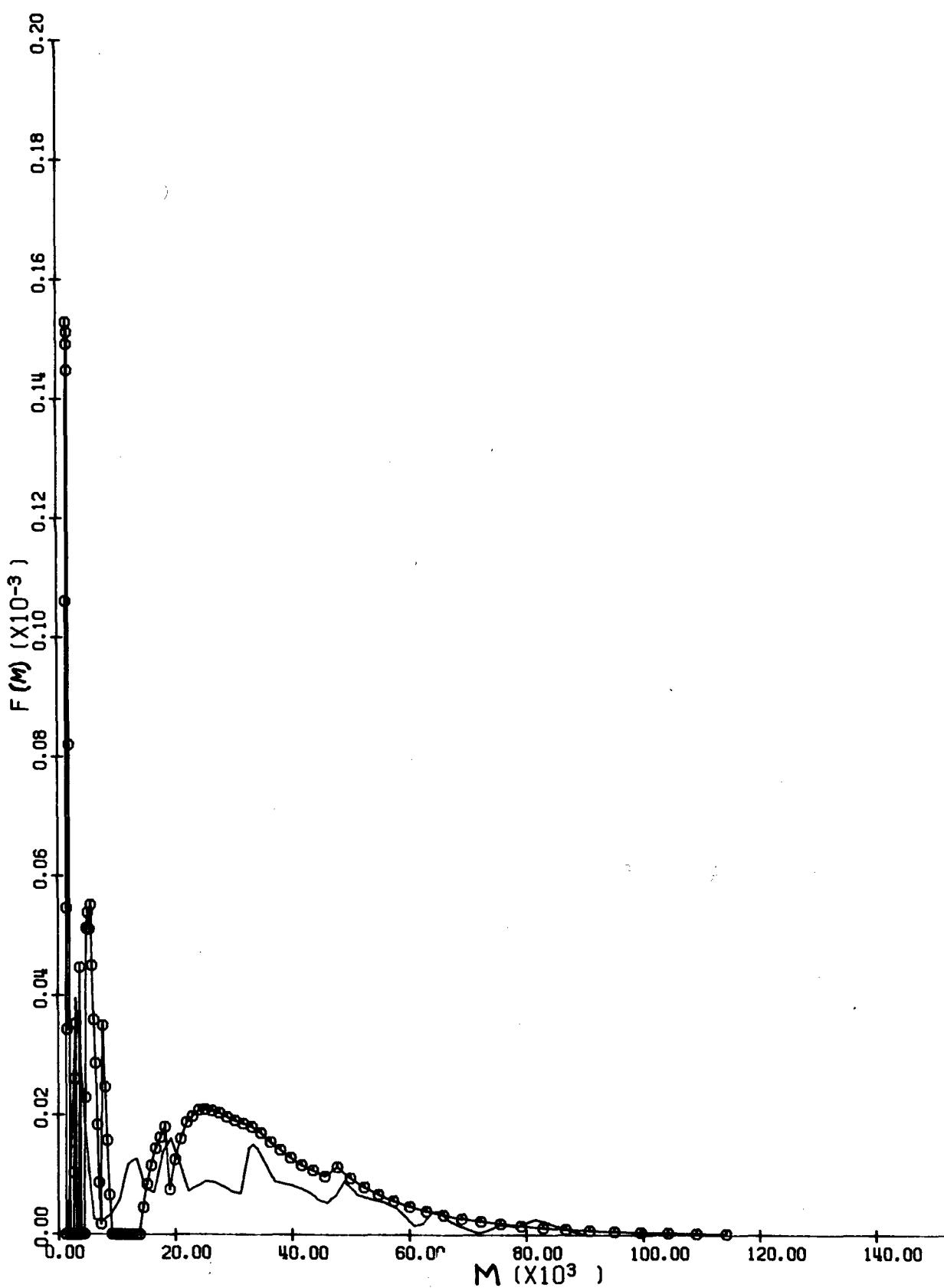


Figure 5. The Effect of Decreasing the MWR on the MWD

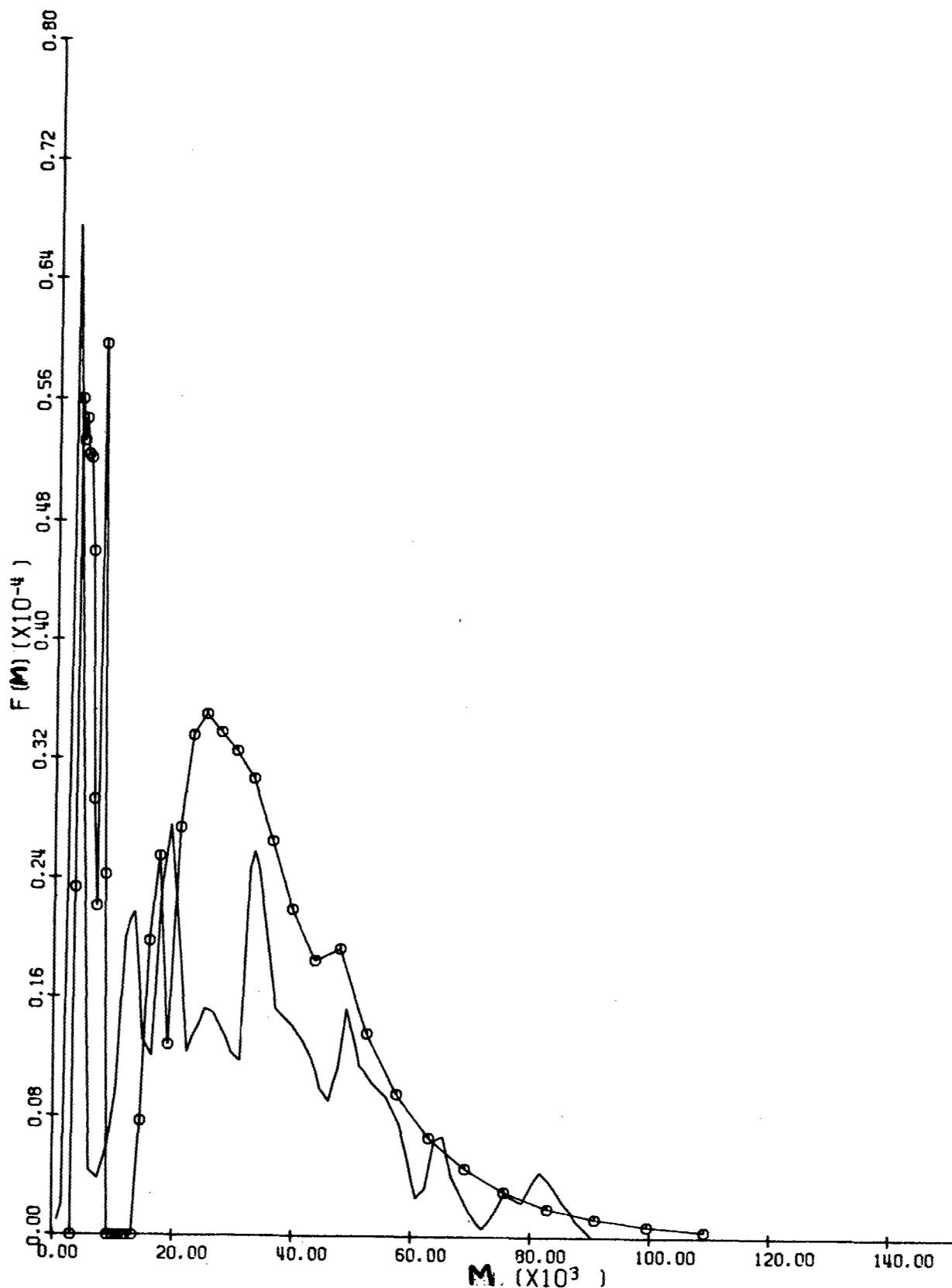


Figure 6. The Effect of Decreasing the MWR and the Number of Molecular Weight Sets on the MWD

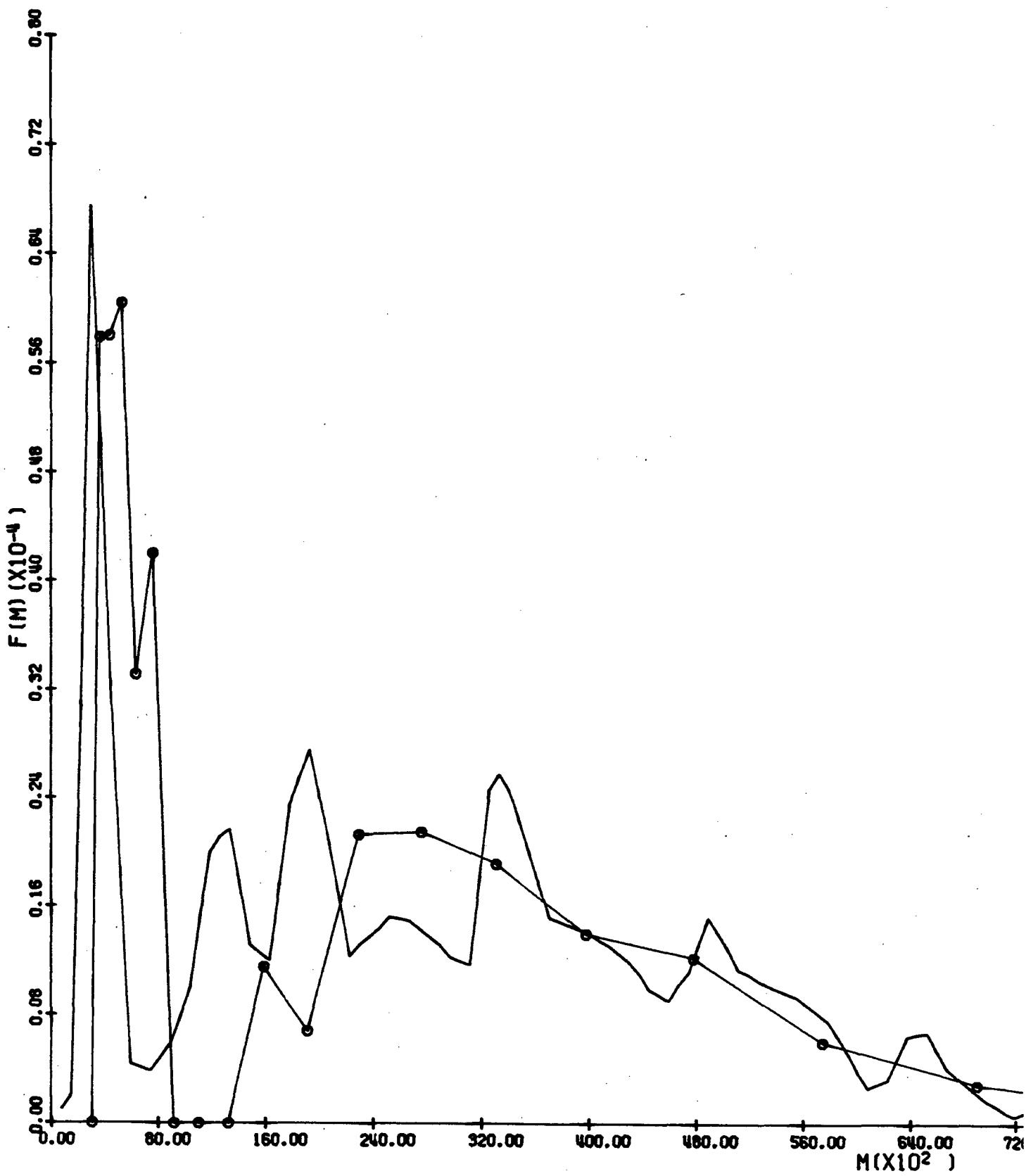
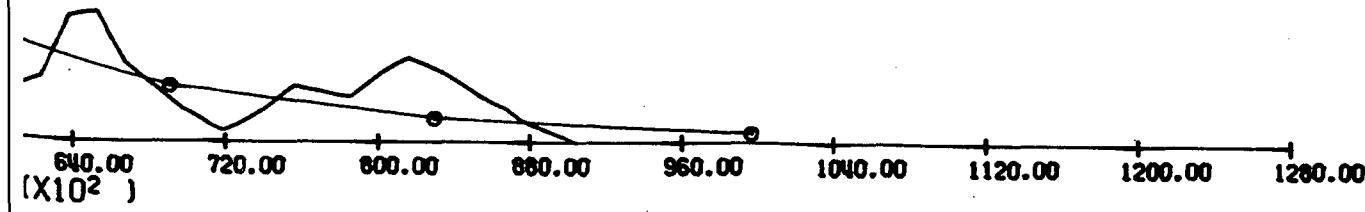


Figure 7. The Effect of Further Decreasing  $t$



or Decreasing the Number of Molecular Weight Sets

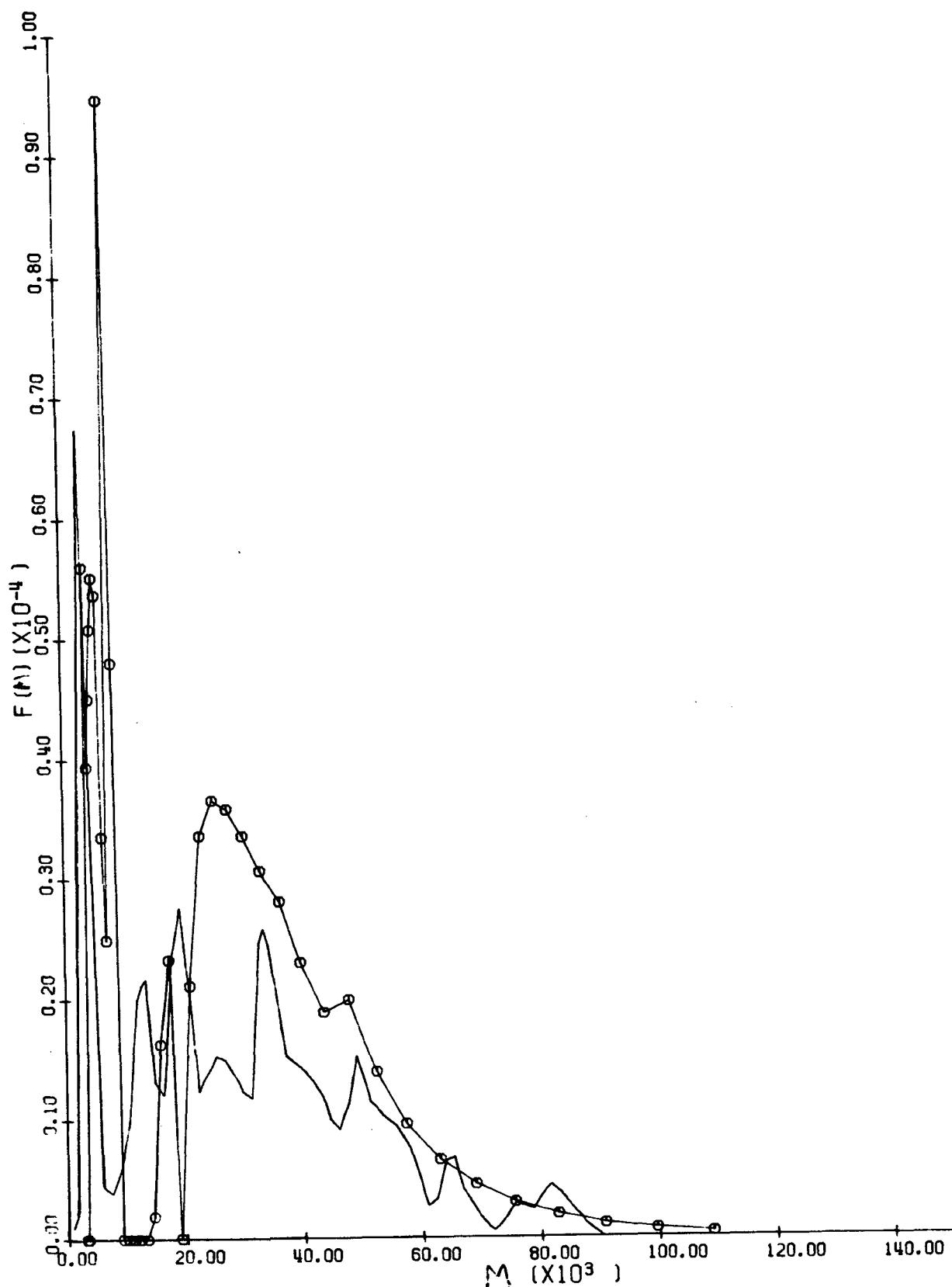


Figure 8. The Effect of Using More Experimental Data on the MWD

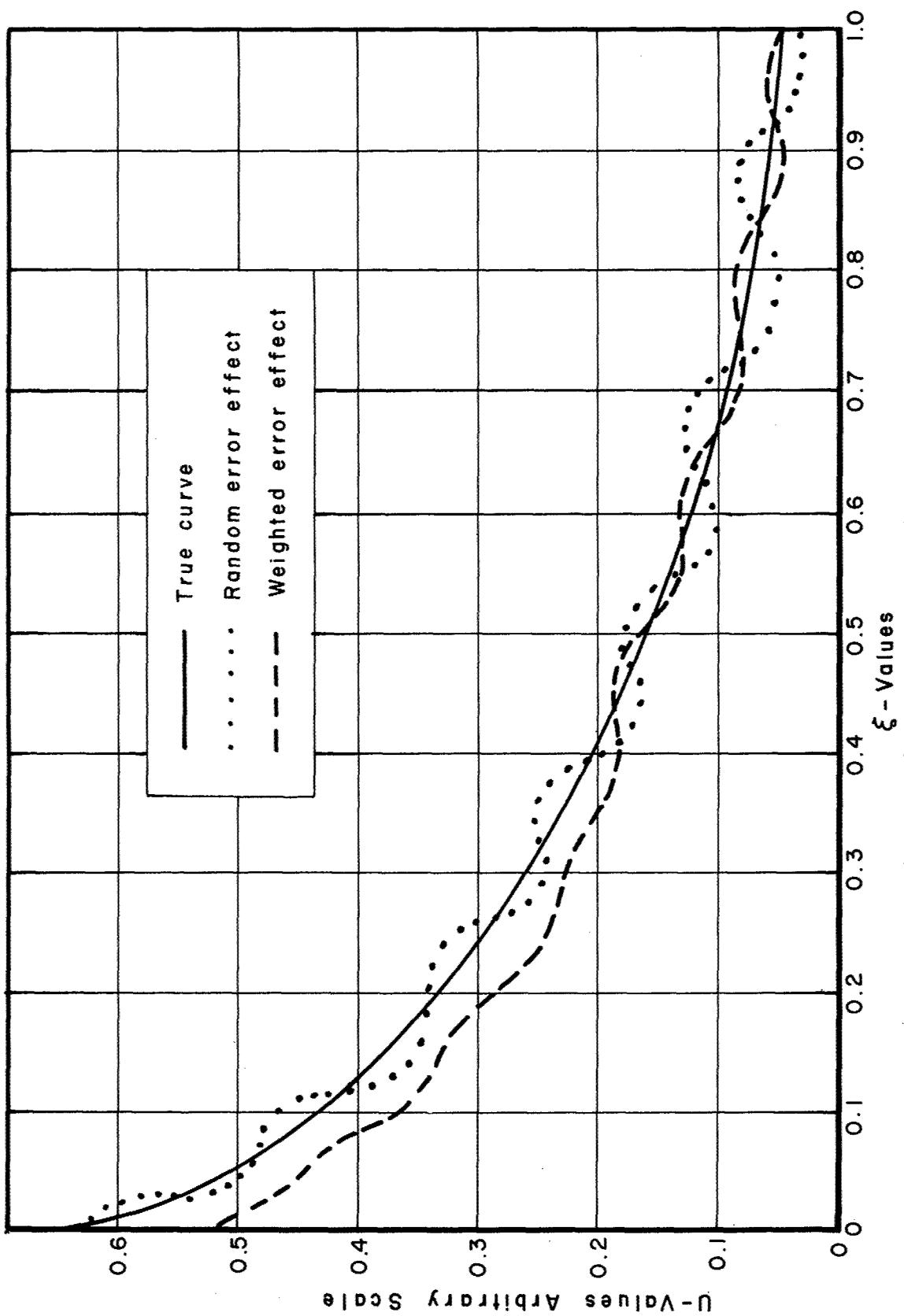


Figure 9. A Typical Curve of Concentration Gradient from One Angular Velocity

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13. ABSTRACT  Within the past decade easy access to high speed digital computers has renewed interest in deriving a molecular weight distribution from equilibrium sedimentation-diffusion data. One of the computational schemes which appears most promising is the Simplex Method of linear programming. The purpose of this work was to investigate the advantages and limitations of this approach.
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It was found that even though inferring a molecular weight distribution from equilibrium sedimentation-diffusion data is mathematically an ill-posed problem, the method of linear programming yields qualitatively a good molecular weight distribution. Also, the method is applicable to the case of one angular velocity.

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Linear Programming						
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Simplex Method						

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